

# The Two-Energies Turbulence Scheme and Length Scale Formulations

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1, 2TE+APDF scheme

2, Budget-Based Turbulence Length Scale Diagnostics

3, TKE scheme in IFS

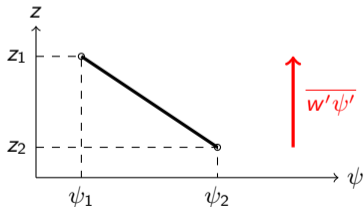
## 2TE+APDF scheme

- ▶ Separate modelling of turbulence and clouds in Atmospheric Boundary Layer (ABL) causes inconsistencies.
- ▶ Unified parameterization of turbulence and clouds should improve the representation of interactions and transition of processes.
- ▶ A parameterization based on **two prognostic turbulence energies** and the **Assumed Probability Density Function** (APDF) approach for modelling both turbulence and clouds is a possible solution.

## Local down-gradient turbulent diffusion

$$\begin{aligned}\overline{u'w'} &= -K_M \frac{\partial u}{\partial z}, & \overline{v'w'} &= -K_M \frac{\partial v}{\partial z}, \\ \overline{\theta'_l w'} &= -K_H \frac{\partial \theta_l}{\partial z}, & \overline{q'_t w'} &= -K_H \frac{\partial q_t}{\partial z},\end{aligned}$$

$K_M$  and  $K_H$  - turbulent diffusion coefficients for momentum and heat/moisture



**Turbulent diffusion coefficients in TKE scheme**

$$\mathbf{K}_M = \frac{\nu^4}{C_\epsilon} \chi_3(Ri_f^*) \sqrt{e_k} L, \quad \mathbf{K}_H = C_3 \frac{\nu^4}{C_\epsilon} \phi_3(Ri_f^*) \sqrt{e_k} L$$

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## Turbulent diffusion coefficients in TKE scheme

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- ▶ TKE - measure of turb. intensity
- ▶ length scale - scale of the problem
- ▶ stability functions - influence of stratification
- ▶ closure constants

$\nu$  - free parameter,  $C_3$  - inverse Prandtl number at neutrality,  $Ri_f^*$  - stability parameter in the form of flux Richardson number:

$$Ri_f \equiv \left( \frac{g}{\theta_v} \overline{\theta'_v w'} \right) / \left( \overline{u' w'} \frac{\partial u}{\partial z} + \overline{v' w'} \frac{\partial v}{\partial z} \right)$$

## Prognostic TKE equation

$$\frac{d\mathbf{e}_k}{dt} = \frac{\partial}{\partial z} \left( K_{e_k} \frac{\partial \mathbf{e}_k}{\partial z} \right) + I + II - \epsilon_k,$$

$$\mathbf{e}_k \equiv \frac{\overline{u'u'} + \overline{v'v'} + \overline{w'w'}}{2} \quad \text{-Turbulence Kinetic Energy (TKE),}$$

$$I \equiv -\overline{u'w'} \frac{\partial u}{\partial z} - \overline{v'w'} \frac{\partial v}{\partial z} \quad \text{-Shear term,}$$

$$II \equiv \frac{g}{\theta_v} \overline{\theta'_v w'} = E_{q_t} \overline{q'_t w'} + E_{\theta_l} \overline{\theta'_l w'} \quad \text{-Buoyancy term}$$

$$\epsilon_k \equiv \frac{2\mathbf{e}_k}{\tau_k} \quad \text{-Dissipation term}$$

$K_{e_k}$  - turb. exchange coefficients for  $e_k$ ;  $\tau_k$  and  $\tau_s$  - are dissipation time scales;  $E_{q_t}$  and  $E_{\theta_l}$  are cloud-dependent weights.

## The two-energies turbulence scheme (2TE)

$$\frac{d\mathbf{e}_k}{dt} = \frac{\partial}{\partial z} \left( K_{e_k} \frac{\partial \mathbf{e}_k}{\partial z} \right) + \boxed{I + II - \frac{2\mathbf{e}_k}{\tau_k}},$$

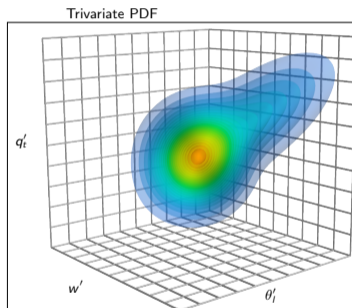
$$\frac{d\mathbf{e}_s}{dt} = \frac{\partial}{\partial z} \left( K_{e_s} \frac{\partial \mathbf{e}_s}{\partial z} \right) + \boxed{I - \frac{2\mathbf{e}_s}{\tau_s}},$$

$$\mathbf{e}_s \equiv \mathbf{e}_k + \frac{E_{q_t} \overline{q_t'^2}}{2 \frac{\partial q_t}{\partial z}} + \frac{E_{\theta_l} \overline{\theta_l'^2}}{2 \frac{\partial \theta_l}{\partial z}},$$

$$Ri_f^{TE} = \frac{\mathbf{e}_s - \mathbf{e}_k}{\mathbf{e}_s + \mathbf{e}_k \left( \frac{C_4}{2C_3} - 1 \right)}$$

$K_{e_s}$  - turb. exchange coefficients for  $e_s$ ;  $\tau_s$  - dissipation time scale

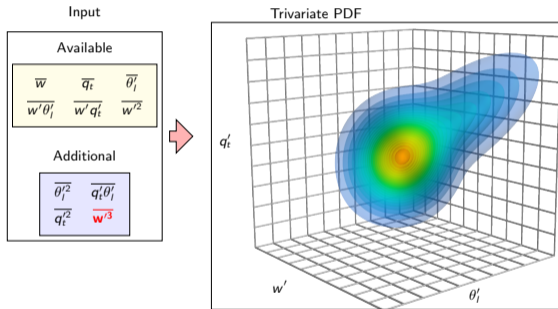
## APDF method



PDF shape given

$C$  - Cloud fraction,  $\theta_v$  - virtual potential temperature

## APDF method

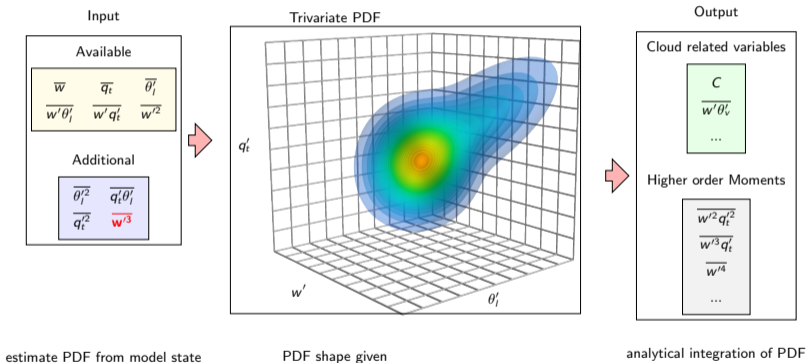


estimate PDF from model state

PDF shape given

C - Cloud fraction,  $\theta_v$  - virtual potential temperature

## APDF method



C - Cloud fraction,  $\theta_v$  - virtual potential temperature

## 2TE+APDF (1)

- ▶ the buoyancy term,  $II$ , is computed via APDF
- ▶ The stability parameter is computed from local gradients ( $Ri_f^{GR}$ ) and turbulence energies:

$$Ri_f^* = C_{Rif} Ri_f^{GR} + (1 - C_{Rif}) Ri_f^{TE}$$

- ▶ Turbulence exchange coefficient for TOMs:

$$K_{ek} = K_{es} = \left( C_{ek} \overline{w'^2} + C_{\theta_s} \frac{g}{\theta_0} \overline{w' \theta'_s} \tau_k \right) \tau_k,$$

$$\overline{w'^3} = -K_{ek} \frac{\partial \overline{w'^2}}{\partial z}$$

$C_{ek}$ ,  $C_{\theta_s}$ , and  $C_{Rif}$  - closure constants,  $Ri_f^{GR} \equiv Ri \frac{K_H}{K_M}$  - computed from conventional gradient Richardson number,  $\overline{w' \theta'_s}$  turbulent flux of the entropy potential temperature (Marquet and Geleyn, 2014)

## 2TE+APDF (2)

- ▶ Canuto et al. (2007) - dry case:

$$\overline{w'^3} = -A_1 \frac{\partial \overline{w'^2}}{\partial z} - A_2 \frac{\partial \overline{w'\theta'}}{\partial z} - A_3 \frac{\partial \overline{\theta'^2}}{\partial z}$$

$$A_1 = \left( a_1 \overline{w'^2} + a_2 \frac{g}{\theta_0} \tau \overline{w'\theta'} \right) \tau$$

- ▶ simplification for moist 2TE+APDF:

$$A_2 = A_3 = 0, \overline{w'\theta'} = \overline{w'\theta'_s}$$



## 2TE+APDF (3)

- Turbulence length scale:

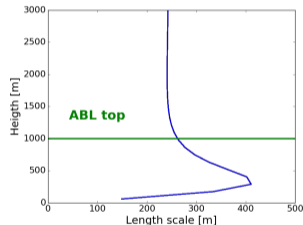
$$L = \frac{(C_K C_\epsilon)^{\frac{1}{4}}}{C_K} \frac{\kappa z}{1 + \frac{\kappa z}{\lambda_m} \left[ \frac{1 + \exp\left(-a_m \sqrt{\frac{z}{H_{abl}} + b_m}\right)}{\beta_m + \exp\left(-a_m \sqrt{\frac{z}{H_{abl}} + b_m}\right)} \right]},$$

$$H_{abl} = C_{ablh} \int_z L_{up} dz,$$

$$\Delta\theta_s > 0 : \beta_m = 0, \quad \Delta\theta_s \leq 0 : \beta_m \neq 0$$

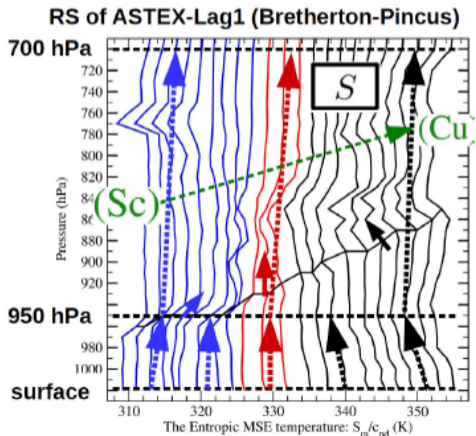
$$\Delta\theta_s = \theta_s(z = 1.5H_{abl}) - \theta_s(z = 0)$$

$\kappa = 0.4$  is the von Kármán constant;  $H_{abl}$  is the ABL height;  $L_{up}$  is upward part of the non-local length scale (Bougeault and Lacarrere, 1989);  $a_m$ ,  $b_m$ ,  $\beta_m$ , and  $\lambda_m$  are shape constants;  $C_{ablh}$  and  $C_K$  are closure constants.



## 2TE+APDF (4)

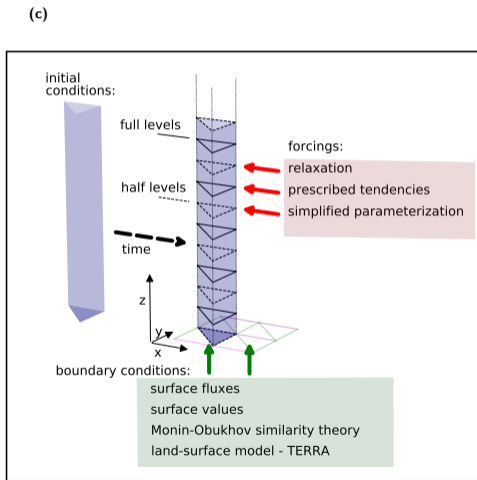
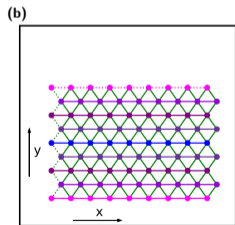
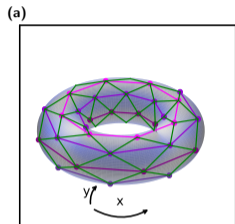
- ▶  $\beta_m \sim$  entrainment
- ▶  $\Delta\theta_s \sim$  entrainment



### ICON experiments

- ▶ Two modes:
  - ▶ **Single Column Mode (SCM)** : Torus grid (8x8), no dynamics
  - ▶ **Cloud Resolving Mode (CRM)** : Torus grid(100x100, 2.5km), with dynamics
- ▶ Two setups:
  - ▶ **NWP** : ICON operational turbulence and convection scheme
  - ▶ **2TE+APDF** : Two-energies scheme with APDF (without convection par.)

## ICON SCM and ICON CRM-PER

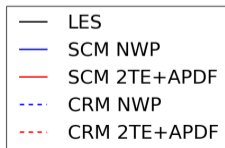
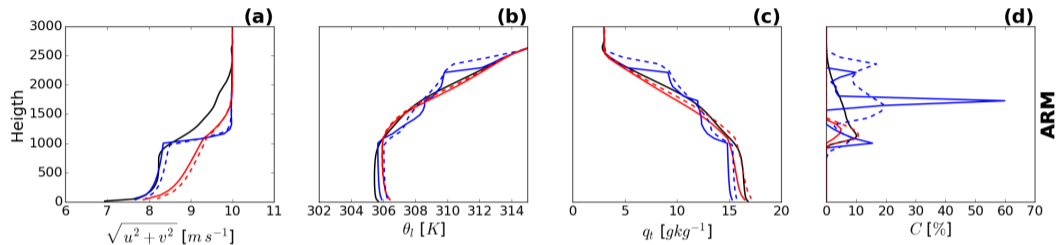


### ICON experiments (2)

- ▶ **MicroHH (van Heerwaarden et al., 2017)** LES is used as reference.
- ▶ Four idealized cases:
  - ▶ **ARM**: Continental shallow,
  - ▶ **BOMEX**: Non-precipitating trade cumulus,
  - ▶ **DYCOMS-II**: Stratocumulus,
  - ▶ **GABLS(1)**: weakly stable stratification

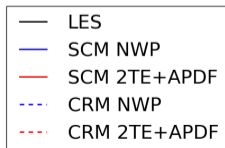
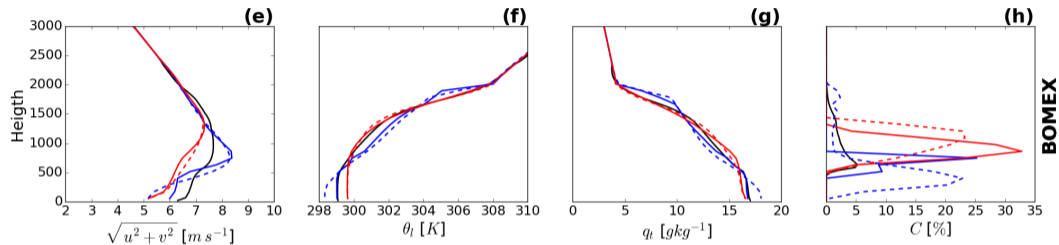
## Vertical profiles after 8 hours of integration

## ARM



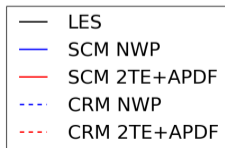
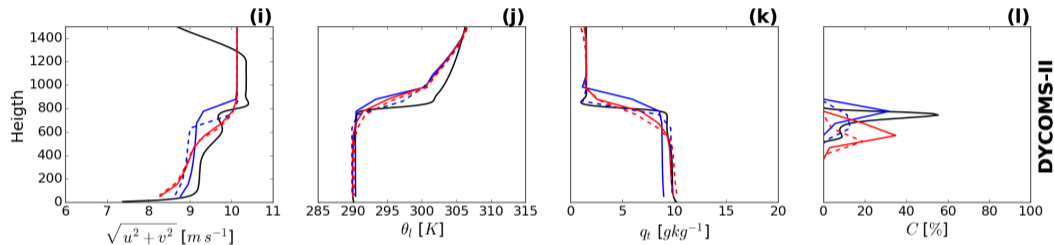
## Vertical profiles after 8 hours of integration

## BOMEX



## Vertical profiles after 8 hours of integration

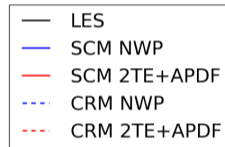
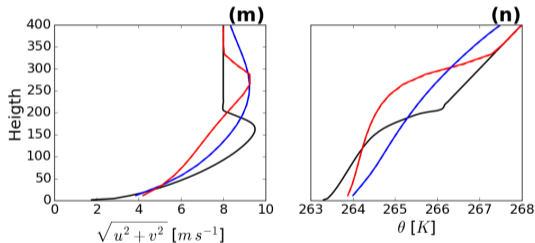
## DYCOMS-II





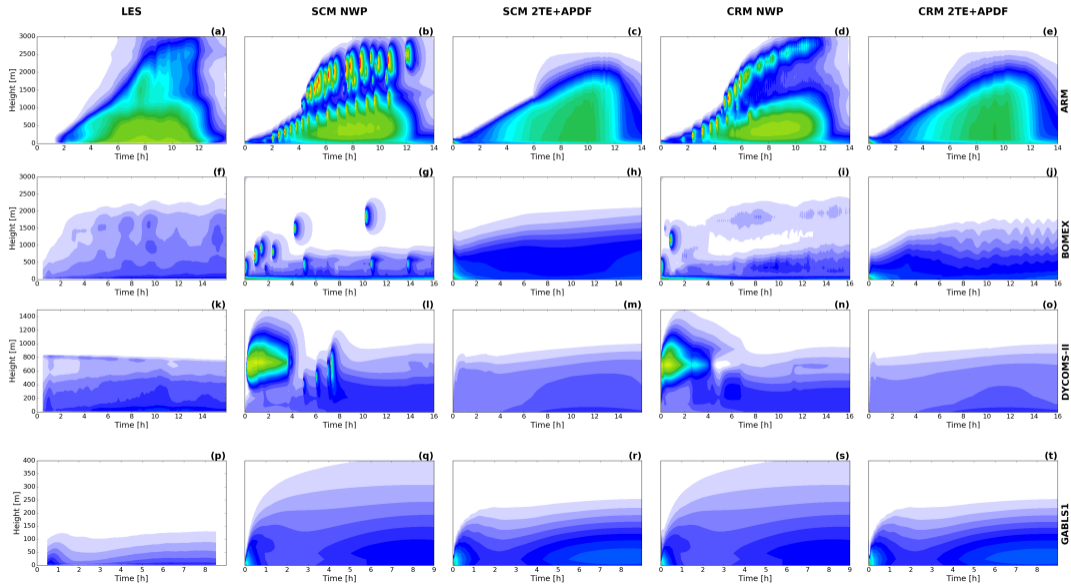
Vertical profiles after 8 hours of integration

GABLS(1)



GABLS1

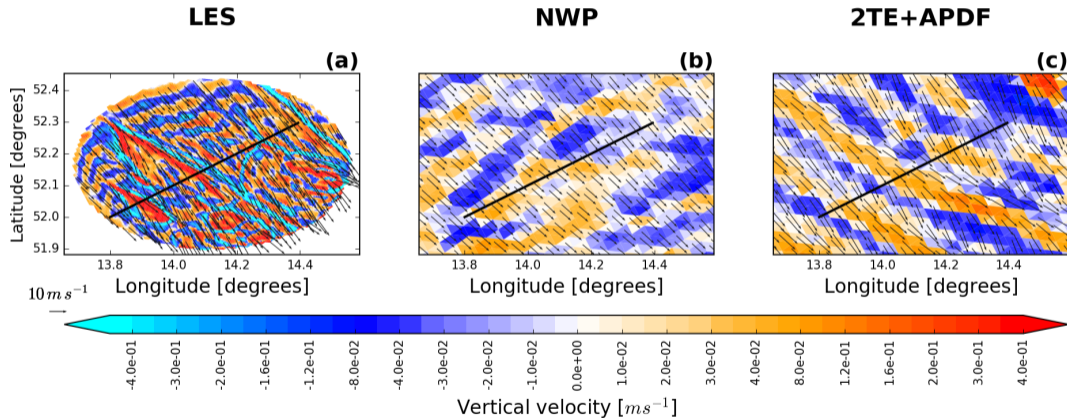
## Evolution of TKE



# 2TE+APDF scheme

Real case - 13.06.2021 : cloud streets

Horizontal cross section at 1900 m



# 2TE+APDF scheme

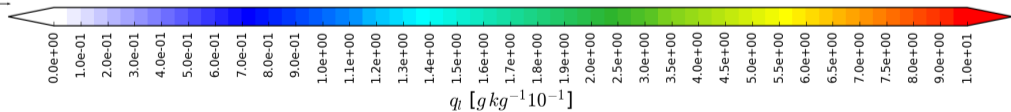
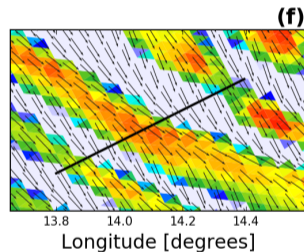
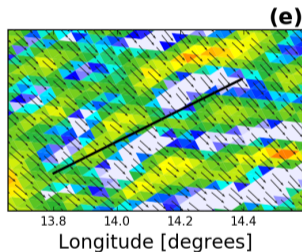
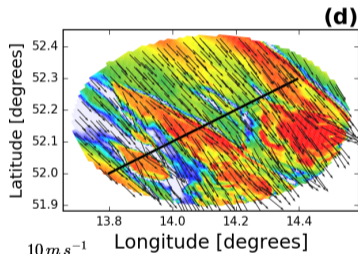
Real case - 13.06.2021 : cloud streets

Horizontal cross section at 1900 m

LES

NWP

2TE+APDF



# 2TE+APDF scheme

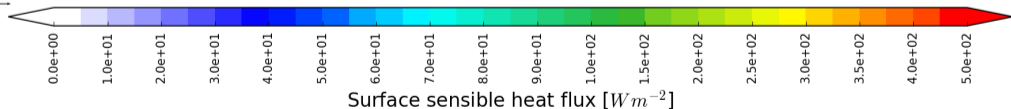
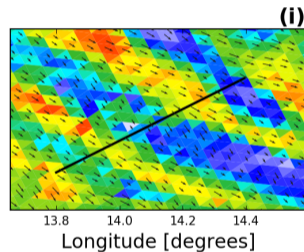
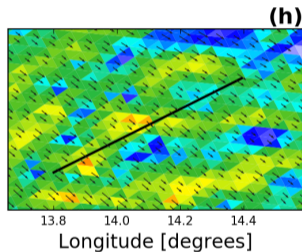
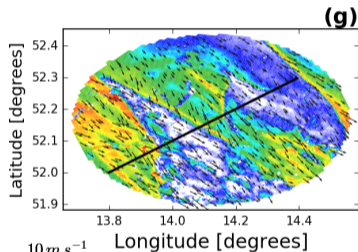
Real case - 13.06.2021 : cloud streets

Horizontal cross section at 1900 m

LES

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# 2TE+APDF scheme

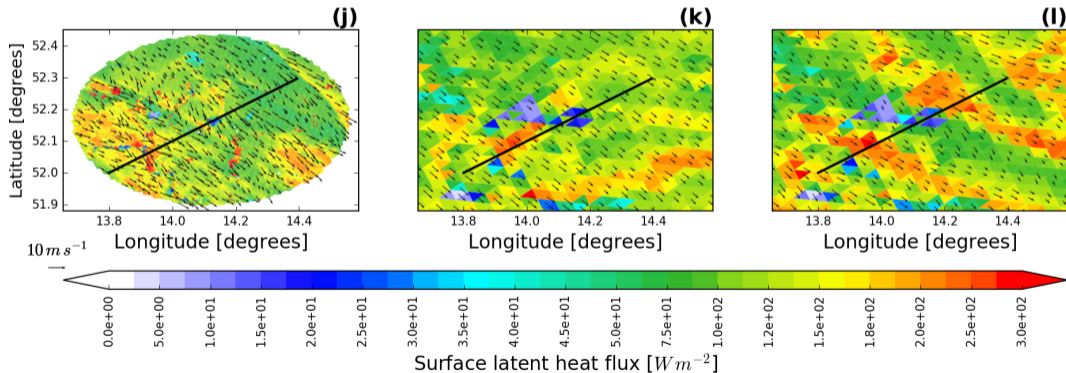
Real case - 13.06.2021 : cloud streets

Horizontal cross section at 1900 m

LES

NWP

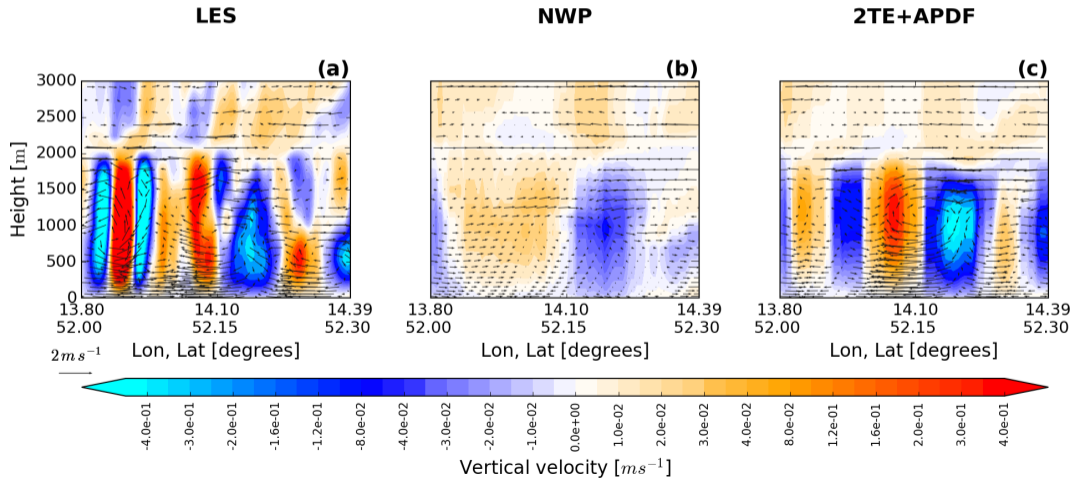
2TE+APDF



# 2TE+APDF scheme

Real case - 13.06.2021 : cloud streets

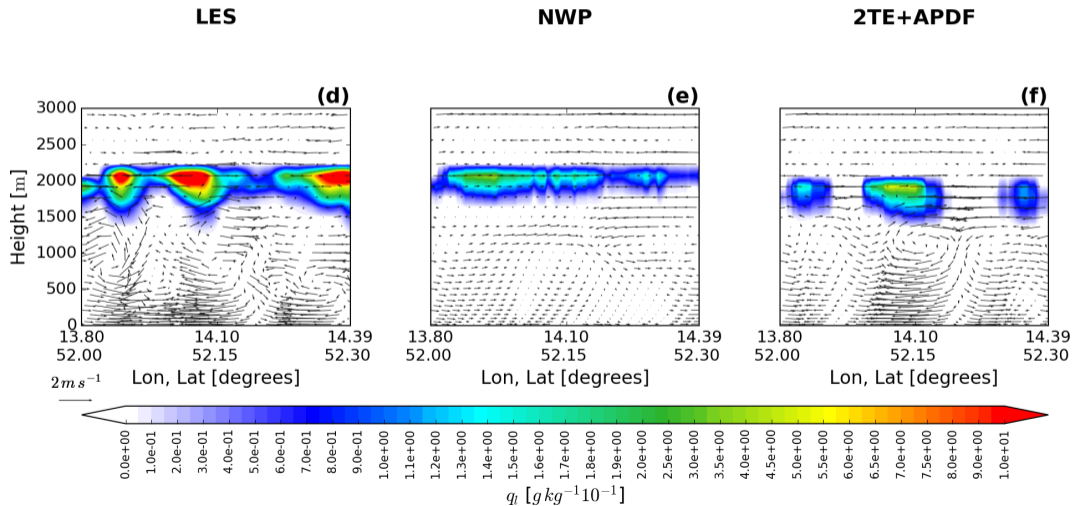
Vertical cross section



# 2TE+APDF scheme

Real case - 13.06.2021 : cloud streets

Vertical cross section

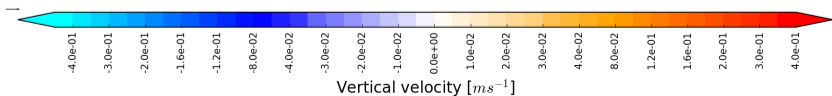
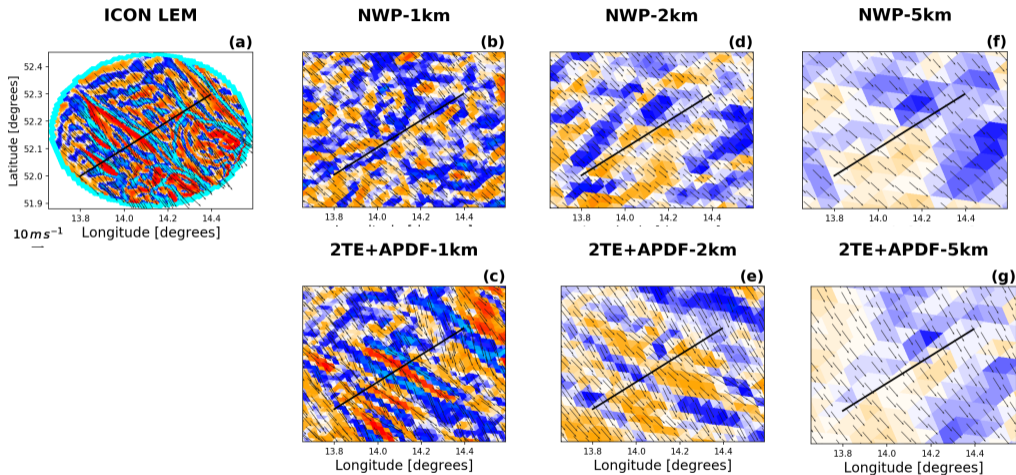




# 2TE+APDF scheme

Real case - 13.06.2021

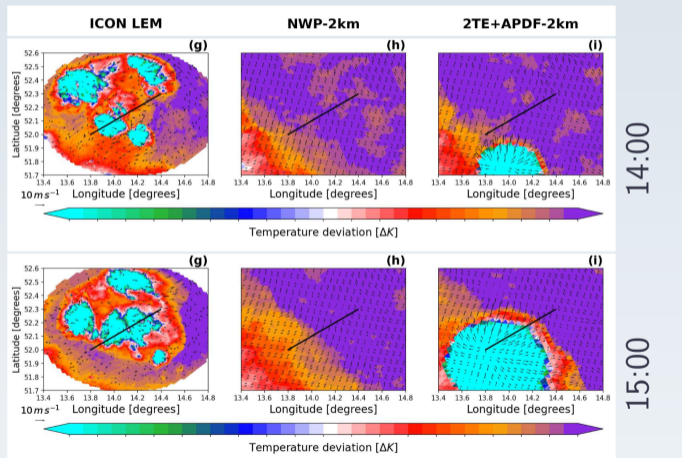
Resolution dependence



# 2TE+APDF scheme

29.06.2021 14:00 and 15:00 - cold pool

Horizontal cross sections - 10 m



### Summary

- ▶ 2TE+APDF scheme is implemented in full ICON code
- ▶ based on selected cases, the 2TE+APDF scheme can be considered as an alternative to the operational turbulence and shallow convection scheme in ICON
- ▶ 2TE+APDF scheme improves the coupling with dynamics, which is beneficial for the modeling of coherent flow structures in the ABL

## Budget-Based Turbulence Length Scale Diagnostics

- ▶ More objective reference for turbulence length scale,  $L$ , is required, especially in the **gray zone** of turbulence, where the **cross-scale transfer** of TKE is not negligible.
- ▶  $L$  can be estimated from the TKE or scalar variance **budget** using high resolution **LES data** (Bastak Duran et al. 2020).

## $L$ diagnostics:

Based on TKE:

$$L_{C,e_k} = \frac{(e_k)^{3/2}}{\tilde{\epsilon}} C_\epsilon$$

where  $\tilde{\epsilon}$  is the **effective molecular dissipation rate**,  $C_\epsilon$  and  $C_p$  are closure constants, and  $e_k$  is the TKE.

Based on scalar variances:

$$L_{C,\phi} = (e_k)^{1/2} \frac{\overline{\phi'^2}}{\tilde{\epsilon}_\phi} \frac{C_\epsilon}{C_p}$$

where  $\phi \in \{q_t, \Theta_l\}$ , and  $\tilde{\epsilon}_\phi$  is the effective molecular dissipation rates of the variance of  $q_t$  and  $\Theta_l$ .

## Five idealized LES cases (Micro-HH LES model):

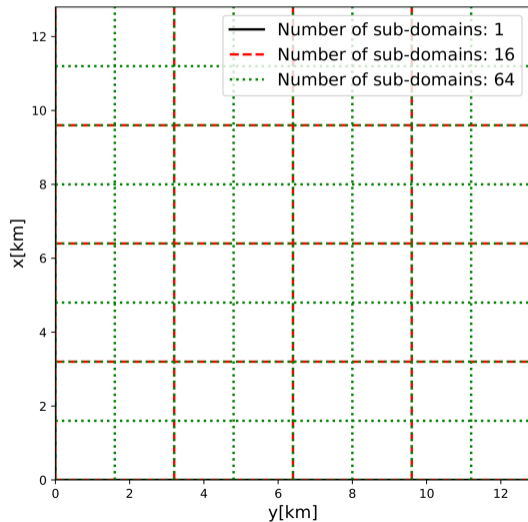
Case	Domain Size ( $km^3$ )	Grid Size ( $m^2$ )
ARM	12.8x12.8x4.4	12.5x12.5x34.4
BOMEX	12.8x12.8x3.0	12.5x12.5x23.4
RICO	12.8x12.8x1.5	12.5x12.5x2.93
DYCOMS-II	12.8x12.8x4.4	12.5x12.5x31.25
GABLS1	0.4x0.4x0.4	12.5x12.5x0.78

The scale dependence is analysed using a coarse graining method of the LES domain.

# Budget-Based Turbulence Length Scale Diagnostics

## Coarse graining method

The scale dependence is analysed using a coarse graining method of the LES domain.



## Length scale formulations

Blackadar (1962) ( $L_B$ ):  $l_B = \frac{k \cdot z}{1 + \frac{k \cdot z}{\lambda}}$ ,

Bastak Duran et al. (2018) ( $L_{BD1}$ ):

$$L_{BD1} = \frac{(C_K \cdot C_\epsilon)^{\frac{1}{4}}}{C_K} \frac{k \cdot z}{1 + \frac{k \cdot z}{\lambda_m} \left[ \frac{1 + \exp\left(-a_m \cdot \sqrt{\frac{z}{H_{abl}}} + b_m\right)}{\beta_m + \exp\left(-a_m \cdot \sqrt{\frac{z}{H_{abl}}} + b_m\right)} \right]},$$

Nakanishi and Niino (2009) ( $L_{NN}$ ):

$$\frac{1}{L_{NN}} = \left( \frac{1}{L_{Surf}} + \frac{1}{L_T} + \frac{1}{L_{Bouy}} \right).$$



## Length scale formulations (2)

Bougeault and Lacarrere (1989) ( $L_{BL}$ ):

$$L_{BL} = \frac{(C_K C_\epsilon)^{\frac{1}{4}}}{C_K} (L_{up} \cdot L_{down})^{\frac{1}{2}},$$
$$\int_z^{z+L_{up}} \frac{g}{\theta_{vr}} (\theta_v(z) - \theta_v(z')) dz' = \mathbf{e}_k(z),$$
$$\int_{z-L_{down}}^z \frac{g}{\theta_{vr}} (\theta_v(z') - \theta_v(z)) dz' = \mathbf{e}_k(z).$$

## Length scale formulations (3)

Honnert et al. (2021) ( $L_{H21}$ ):

$$L_{H21} = \min(L_R, \alpha \cdot L_{LES}),$$

$$L_{LES} = (\Delta x \cdot \Delta y)^{\frac{1}{2}}$$

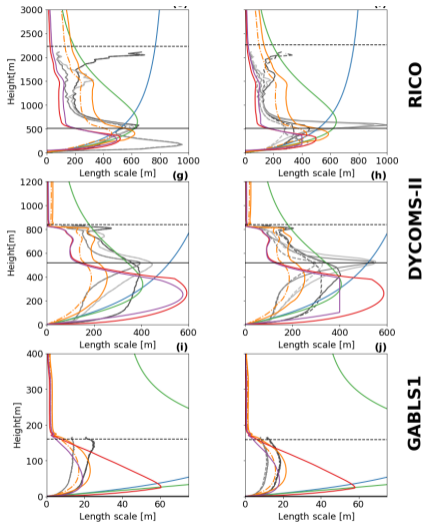
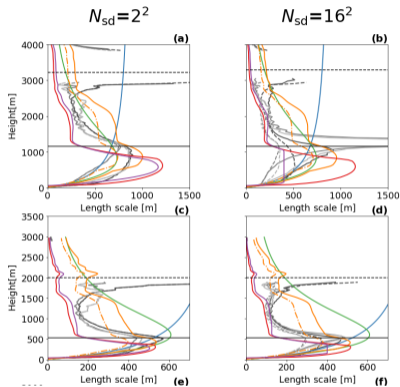
$$L_R = \frac{(C_K C_\epsilon)^{\frac{1}{4}}}{C_K} \left( \frac{L_{Rup}^{-\frac{2}{3}} + L_{Rdown}^{-\frac{2}{3}}}{2} \right)^{-\frac{3}{2}},$$

$$\int_z^{z+L_{Rup}} \frac{g}{\theta_{vr}} (\theta_v(z) - \theta_v(z') + \mathbf{C}_0 \cdot \sqrt{\mathbf{e}_k} \cdot \sigma(\mathbf{z}')) dz' = \mathbf{e}_k(z),$$

$$\int_{z-L_{Rdown}}^z \frac{g}{\theta_{vr}} (\theta_v(z) - \theta_v(z') + \mathbf{C}_0 \cdot \sqrt{\mathbf{e}_k} \cdot \sigma(\mathbf{z}')) dz' = \mathbf{e}_k(z),$$

# Budget-Based Turbulence Length Scale Diagnostics

## Vertical profiles



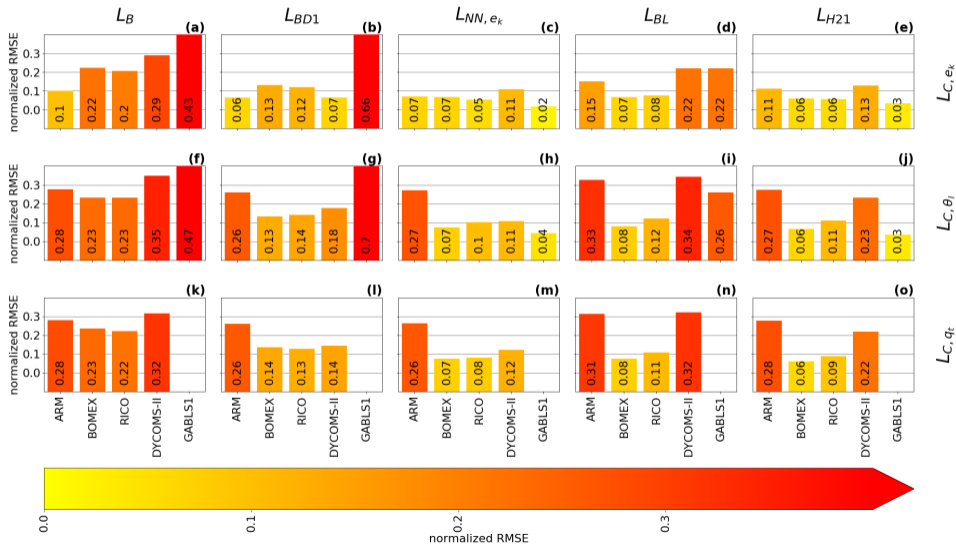
## Normalized (by $H_{abl}$ ) RMSE

$$\text{RMSE}_n = \sqrt{\frac{1}{n_z n_t} \sum_{j=1}^{j=n_t} \sum_{i=1}^{i=n_z} \left( \frac{L_F(z_i, t_j) - L_D(z_i, t_j)}{H_{abl}} \right)^2},$$

$z_i$  is the height of the  $i$ -th model level,  $n_z$  is number of model levels in the ABL,  $t_j$  is the time after  $j$  time steps,  $n_t$  is number of time steps,  $L_F$  is an algebraic length scale,  $L_D$  is diagnosed length scale.

# Budget-Based Turbulence Length Scale Diagnostics

## Normalized RMSE



## Three-component score

Amplitude:

$$\mathbf{A} = \frac{1}{n_t} \sum_{j=1}^{j=n_t} (L_{FP}(t_j) - L_{DP}(t_j)),$$

$$L_{FP} = \frac{1}{H_{abl}^2} \int_{z=0}^{z=H_{abl}} L_F(z) dz, \quad L_{DP} = \frac{1}{H_{abl}^2} \int_{z=0}^{z=H_{abl}} L_D(z) dz,$$

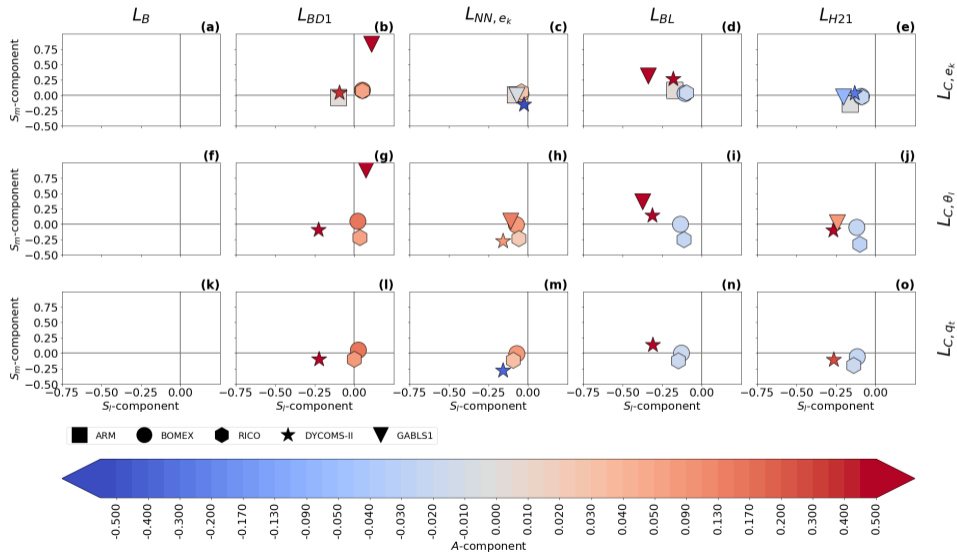
Peak location and magnitude:

$$\mathbf{S}_l = \frac{1}{n_t} \sum_{j=1}^{j=n_t} \frac{z_{F,max}(t_j) - z_{D,max}(t_j)}{H_{abl}},$$

$$\mathbf{S}_m = \frac{1}{n_t} \sum_{j=1}^{j=n_t} \frac{L_{F,max}(t_j) - L_{D,max}(t_j)}{H_{abl}},$$

# Budget-Based Turbulence Length Scale Diagnostics

## Three-component score



## Summary

- ▶  $L$  can be estimated from LES data using budget based diagnostic (Bastak Duran et al. 2020).
- ▶ Typical shape of  $L$ : proportional to the distance from surface near surface, peak in the ABL, asymptotic value (positive or zero) at the top of the ABL.
- ▶  $TKE$ -based  $L$  formulations show better performance.



## TKE scheme in IFS

- ▶ TKE scheme from ARPEGE physics (CBR scheme) already implemented
- ▶ Calibration in IFS is required:
  - ▶ **Under-estimation of turbulent mixing in free atmosphere - particularly tropical jet region**
  - ▶ Under-estimation of Stratocumulus cloudiness
  - ▶ ...

## TKE in free atmosphere

- ▶ TKE source terms are computed using TKE from previous time step:

$$\text{Shear term} = K_M (\mathbf{e}_k^-) \cdot S^2, \text{ Buoyancy term} = K_H (\mathbf{e}_k^-) \cdot N^2$$

- ▶ Problem with **temporal discretization**:  $e_k^- = 0 \Rightarrow e_k^+ = 0$

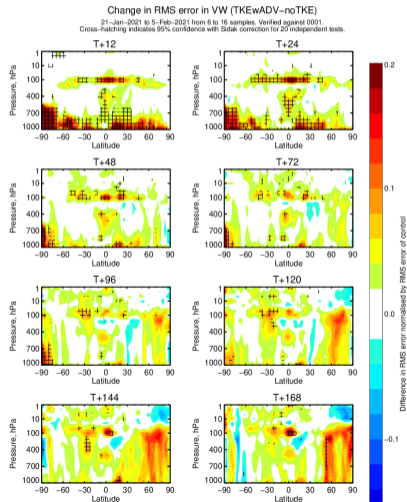
- ▶ Solution: assume **TKE equilibrium** to estimate the TKE source terms:

$$\text{Shear term} = K_M (\tilde{\mathbf{e}}_k) \cdot S^2, \text{ Buoyancy term} = K_H (\tilde{\mathbf{e}}_k) \cdot N^2$$

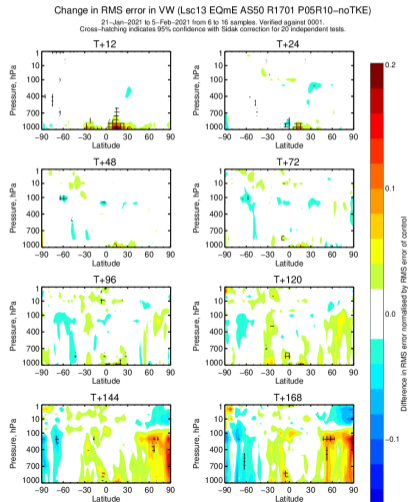
# TKE scheme in IFS

## TKE in free atmosphere (change in RMSE of wind vector)

### Original implementation



### Equilibrium TKE source terms



Thank you for your attention!