

Planetary Boundary Layer 2

Fundamental concepts

Annelize van Niekerk, Irina Sandu, Anton Beljaars

Annelize.vanNiekerk@ecmwf.int

Contents

- Local eddy diffusion (k-profile)
- Surface layer similarity theory
- Roughness length
- Outer layer local eddy diffusion
- Non-local mass flux in convective PBLs

Set of equations to solve in the model

Momentum

$$\frac{\partial \bar{u}}{\partial t} = -\frac{1}{\rho} \left[\nabla \cdot (\rho \bar{u} \mathbf{u}) + \frac{\partial \overline{\rho u' w'}}{\partial z} \right] + f v - \frac{1}{\rho} \frac{\partial p}{\partial x}$$

$$\frac{\partial \bar{v}}{\partial t} = -\frac{1}{\rho} \left[\nabla \cdot (\rho \bar{v} \mathbf{u}) + \frac{\partial \overline{\rho v' w'}}{\partial z} \right] - f u - \frac{1}{\rho} \frac{\partial p}{\partial y}$$

$$\frac{\partial \bar{p}}{\partial z} = -\rho g$$

Large scale terms – resolved by model

Small scale turbulent fluxes – must be parametrized

Sources and sinks (e.g. heating and cooling from radiation)

Thermodynamics

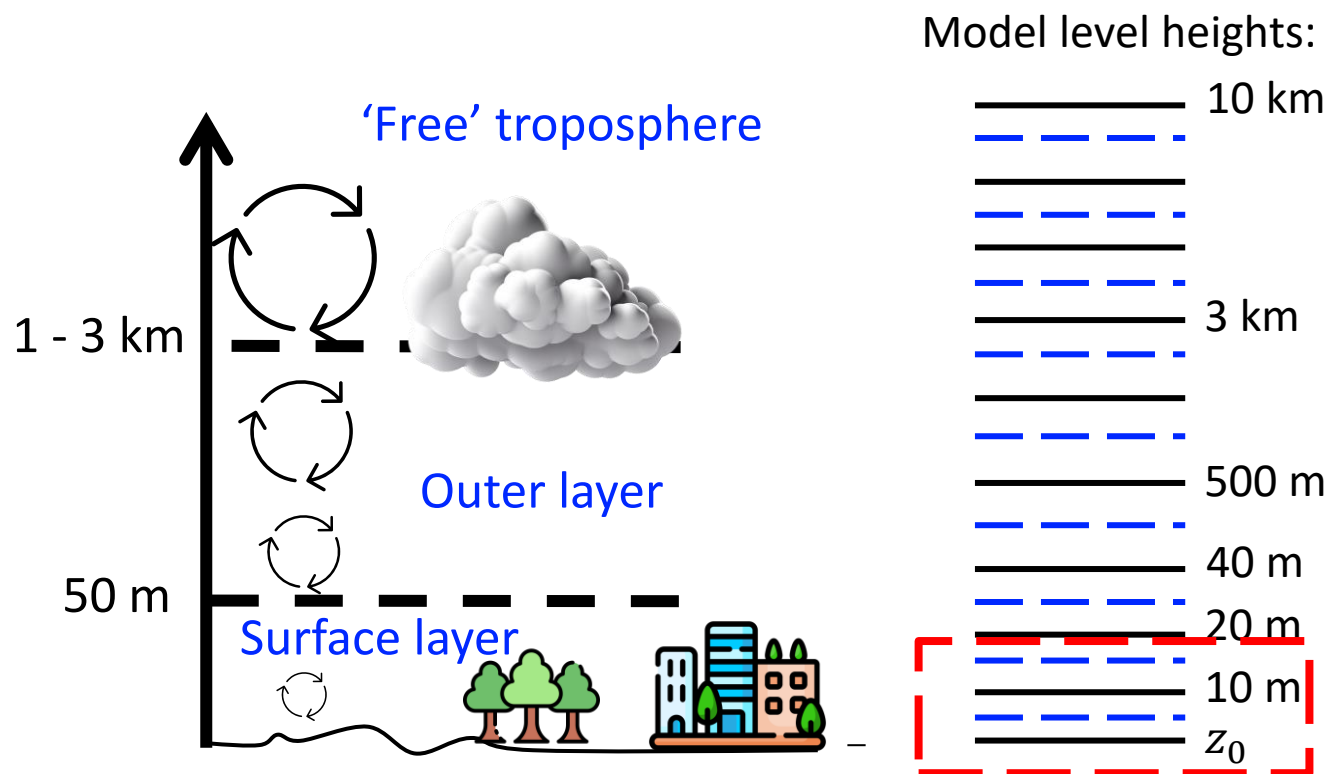
$$\frac{\partial \bar{\theta}}{\partial t} = -\frac{1}{\rho} \left[\nabla \cdot (\rho \bar{\theta} \mathbf{u}) + \frac{\partial \overline{\rho \theta' w'}}{\partial z} \right] + S_{\theta}$$

Moisture

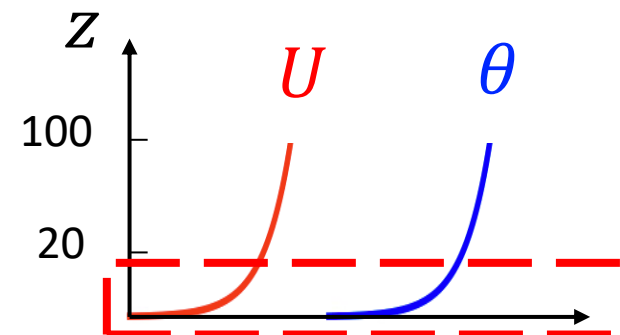
$$\frac{\partial \bar{q}}{\partial t} = -\frac{1}{\rho} \left[\nabla \cdot (\rho \bar{q} \mathbf{u}) + \frac{\partial \overline{\rho q' w'}}{\partial z} \right] + S_q$$

What do we need from a BL turbulence parametrization?

- Provide turbulent fluxes of heat, momentum, moisture (and tracers) between the surface and the upper atmosphere
- Provide turbulent mixing throughout the entire atmosphere – the mixed layer, the cloud layer and the stratosphere
- Account for differences in stability, surface properties and clouds
- Provide profiles of winds and temperatures at the surface, where the model does not resolve in the vertical



- Model does not resolve surface layer
- There are strong gradients and is where people live
- Requires diagnosis of profiles below 10m



‘Local’ turbulence closure: eddy
diffusion (K-profile)

'Local' turbulence closure: eddy diffusion (K-profile)

Momentum

$$\frac{\partial \bar{u}}{\partial t} = -\frac{1}{\rho} \left[\frac{\partial \overline{\rho u' w'}}{\partial z} \right]$$

Thermodynamics

$$\frac{\partial \bar{\theta}}{\partial t} = -\frac{1}{\rho} \left[\frac{\partial \overline{\rho \theta' w'}}{\partial z} \right]$$

Moisture

$$\frac{\partial \bar{q}}{\partial t} = -\frac{1}{\rho} \left[\frac{\partial \overline{\rho q' w'}}{\partial z} \right]$$

'Local' turbulence closure: eddy diffusion (K-profile)

Momentum

$$\frac{\partial \bar{u}}{\partial t} = -\frac{1}{\rho} \left[\frac{\partial \overline{\rho u' w'}}{\partial z} \right] \sim -\frac{1}{\rho} \frac{\partial}{\partial z} \left(-\rho K_M \frac{\partial \bar{u}}{\partial z} \right)$$

K_M , K_H and K_q are the exchange coefficients of momentum, heat and moisture

Their magnitude determines the transfer of these conserved quantities by turbulent eddies

Thermodynamics

$$\frac{\partial \bar{\theta}}{\partial t} = -\frac{1}{\rho} \left[\frac{\partial \overline{\rho \theta' w'}}{\partial z} \right] \sim -\frac{1}{\rho} \frac{\partial}{\partial z} \left(-\rho K_H \frac{\partial \bar{\theta}}{\partial z} \right)$$

Moisture

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'Local' turbulence closure: eddy diffusion (K-profile)

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Generally assumed that diffusion of heat == diffusion of moisture

$$K_H = K_q$$

'Local' turbulence closure: eddy diffusion (K-profile)

Momentum

$$\frac{\partial \bar{u}}{\partial t} = -\frac{1}{\rho} \left[\frac{\partial \overline{\rho u' w'}}{\partial z} \right] \sim -\frac{1}{\rho} \frac{\partial}{\partial z} \left(-\rho K_M \frac{\partial \bar{u}}{\partial z} \right)$$

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K_M , K_H and K_q are the exchange coefficients of momentum, heat and moisture

Their magnitude determines the transfer of these conserved quantities by turbulent eddies

'Local' turbulence closure: eddy diffusion (K-profile)

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z}$$

Thermodynamics

$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z}$$

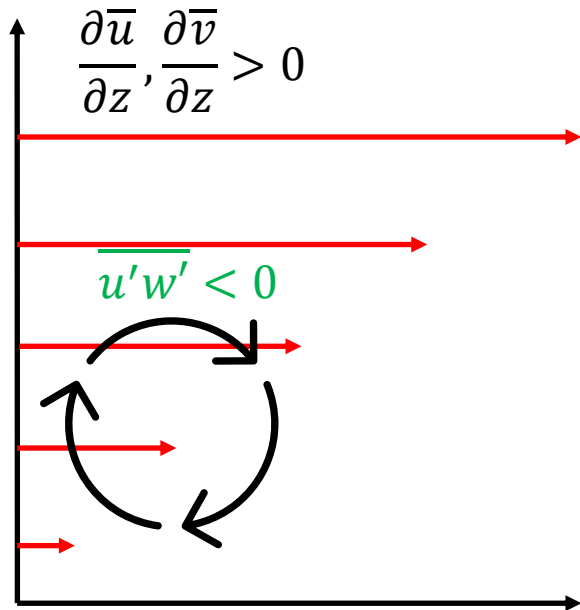
K_M , K_H and K_q are the exchange coefficients of momentum, heat and moisture

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'Local' turbulence closure: eddy diffusion (K-profile)

Momentum

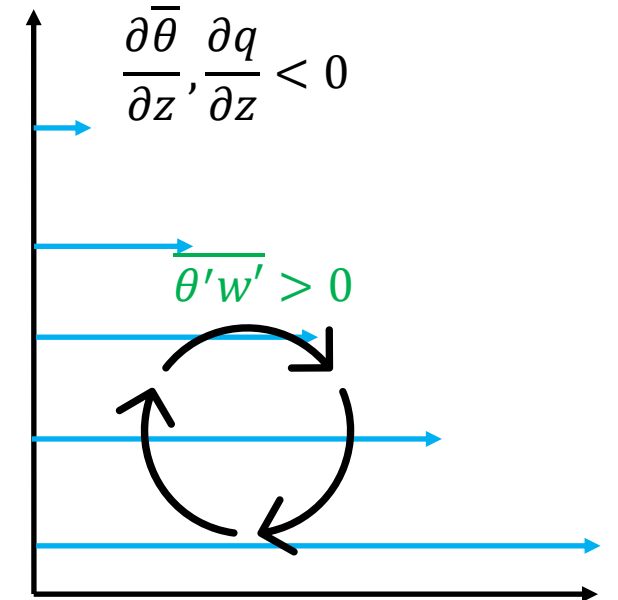
$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z}$$



Wind / temperature gradient with turbulent eddies will generate mixing

Thermodynamics

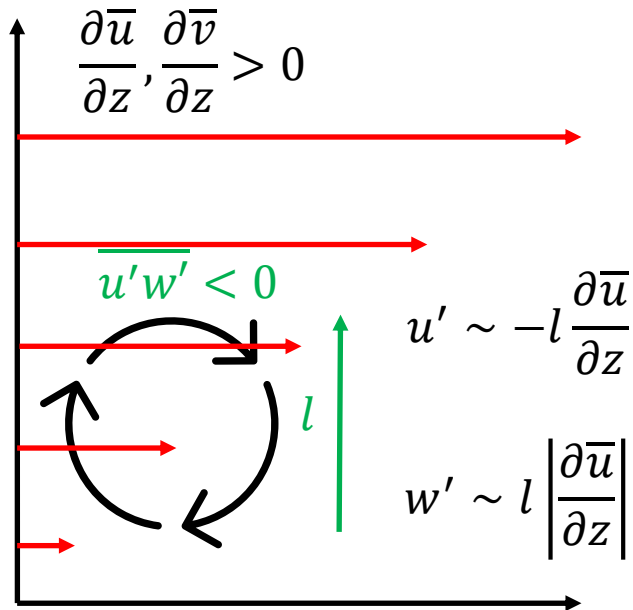
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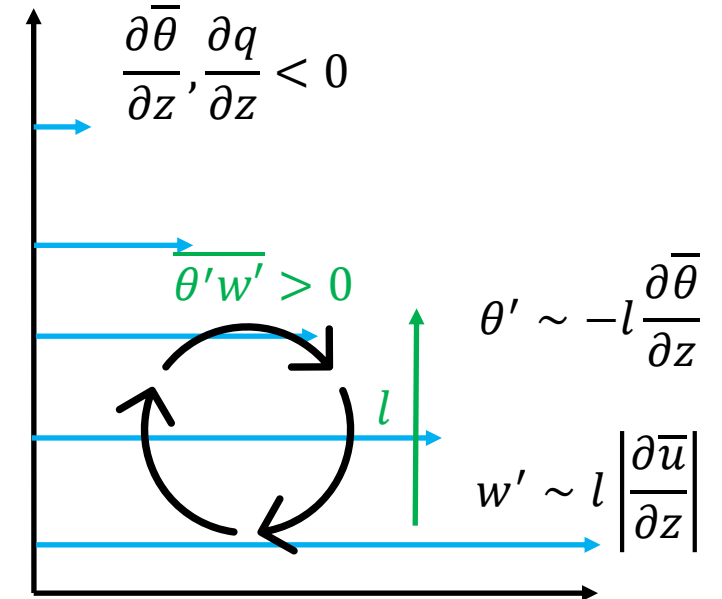


Wind / temperature gradient with turbulent eddies will generate mixing

Mixing occurs over a certain lengthscale l , related to size of eddies

Thermodynamics

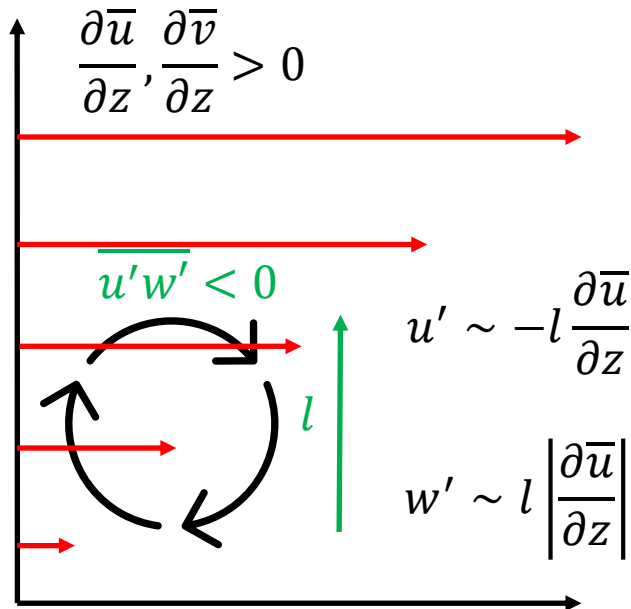
$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z}$$



'Local' turbulence closure: eddy diffusion (K-profile)

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$



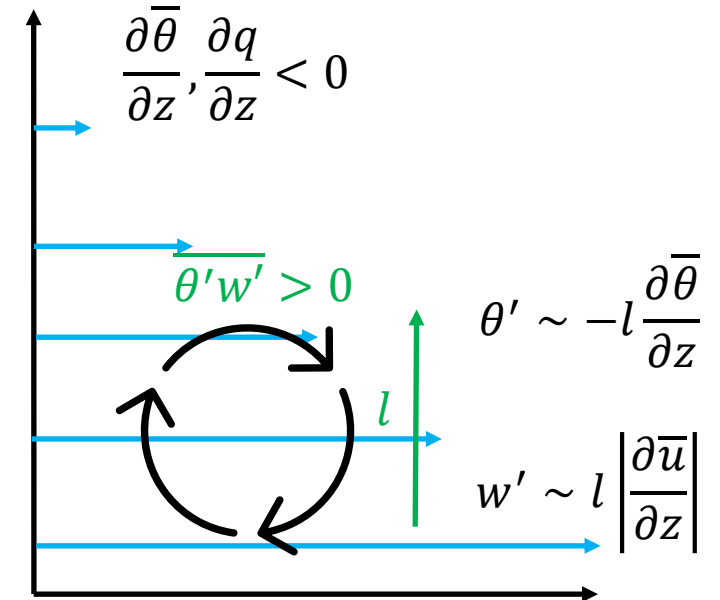
Wind / temperature gradient with turbulent eddies will generate mixing

Mixing occurs over a certain lengthscale l , related to size of eddies

This lengthscale can be used to determine the exchange coefficients

Thermodynamics

$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{\theta}}{\partial z}$$

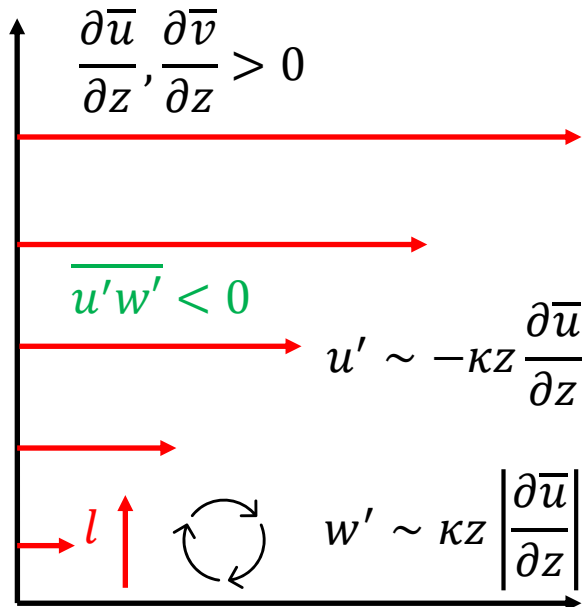


'Local' turbulence closure at the surface

What is l at the surface?

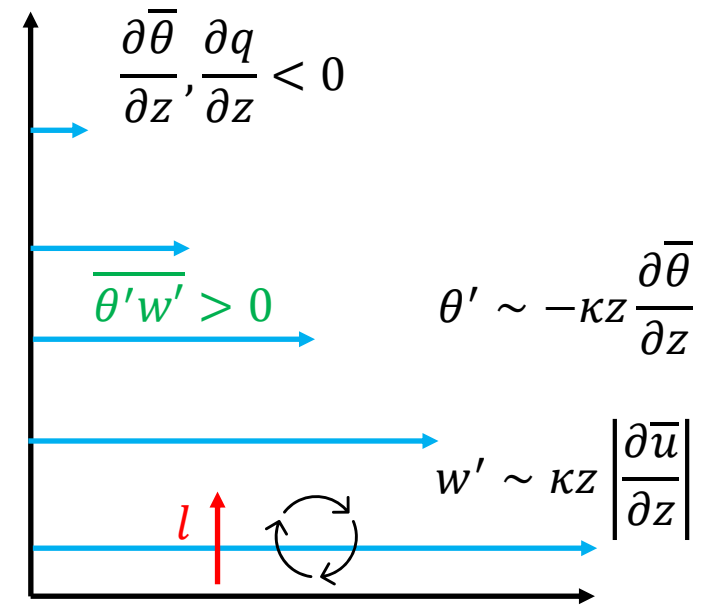
Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$



Thermodynamics

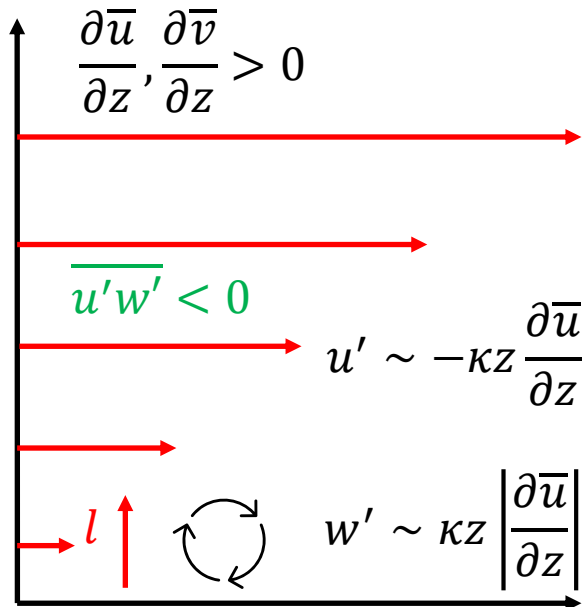
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$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$



Size of eddies are constrained by the surface itself:

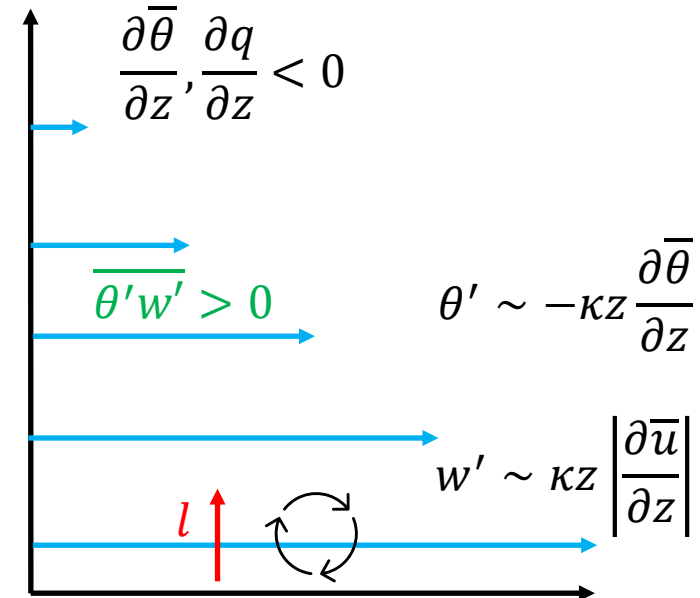
$$l \sim \kappa z,$$

$$\kappa \sim 0.4$$

von-Karman constant
– determined from observations

Thermodynamics

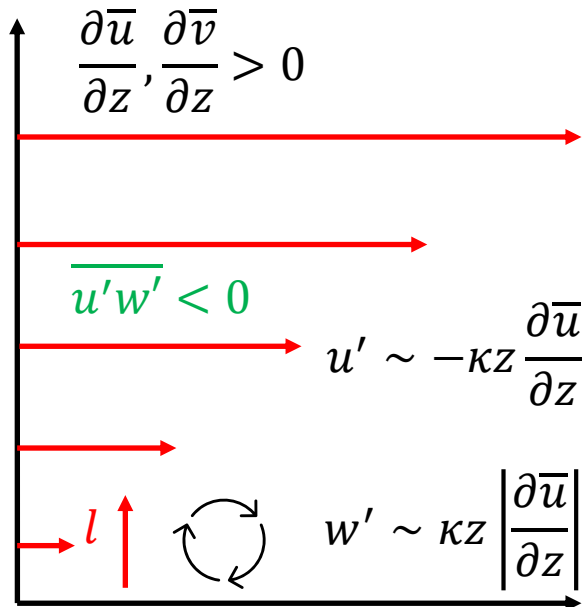
$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z} = -l^2 \left| \frac{\partial \bar{\theta}}{\partial z} \right| \frac{\partial \bar{\theta}}{\partial z}$$



What is l at the surface?

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -\kappa^2 z^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$



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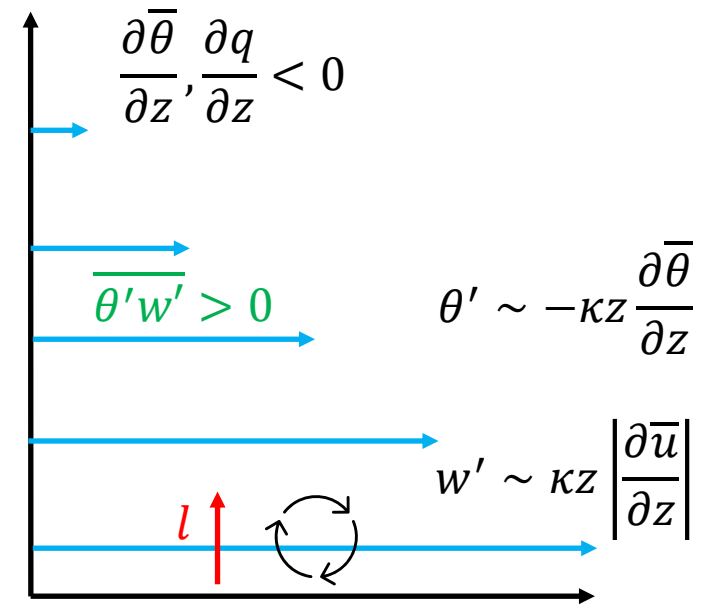
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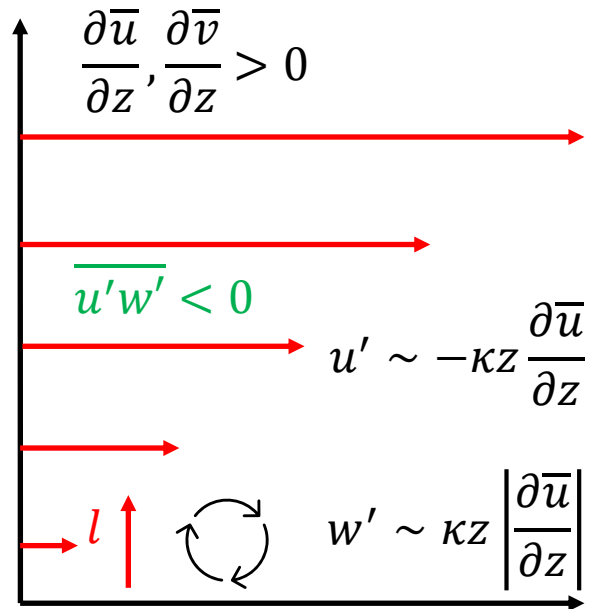
Assume that fluxes are constant with height

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -\kappa^2 z^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$

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Near surface, fluxes are assumed constant with height $(\overline{u'w'})_z = (\overline{u'w'})_s$:

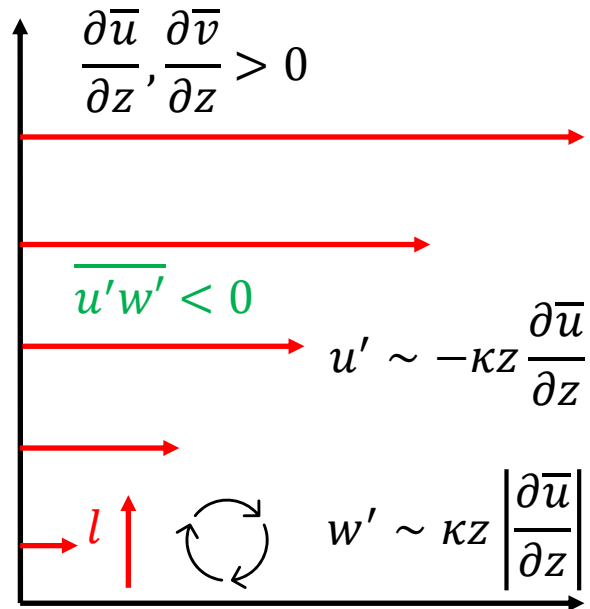
Assume that fluxes are constant with height

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Thermodynamics

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Near surface, fluxes are assumed constant with height $(\overline{u'w'})_z = (\overline{u'w'})_s$:

$$(\overline{u'w'})_z = -\kappa^2 z^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z} = u_*^2$$

$$(\overline{\theta'w'})_z = -\kappa^2 z^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{\theta}}{\partial z} = u_* \theta_*$$

Where $u_* = \sqrt{(\overline{u'w'})_s} = \kappa z \left| \frac{\partial \bar{u}}{\partial z} \right|$ is the surface frictional velocity

θ_* is the temperature scaling, similarly, q_* is the moisture scaling

This means we can get profiles of \bar{u} and $\bar{\theta}$ from flux

Momentum

$$\overline{u'w'} = u_*^2 = -\kappa^2 z^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$

Thermodynamics

$$\overline{\theta'w'} = \theta_* u_* = -\kappa^2 z^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{\theta}}{\partial z}$$

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Momentum

$$\kappa z \frac{\partial \bar{u}}{\partial z} = u_*$$

Thermodynamics

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Momentum

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Integrate:

$$\bar{u}_z - \bar{u}_s = \frac{u_*}{\kappa} \int_{z_0}^{z+z_0} \frac{1}{z} dz$$

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θ_* is the **temperature scaling**,
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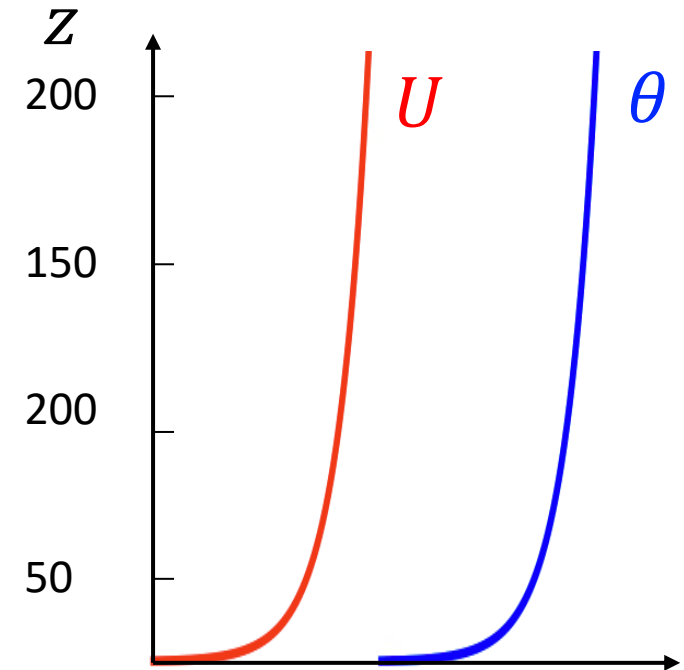
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$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \log \left(\frac{z + z_0}{z_0} \right)$$

Gives log profile for winds and potential temperature



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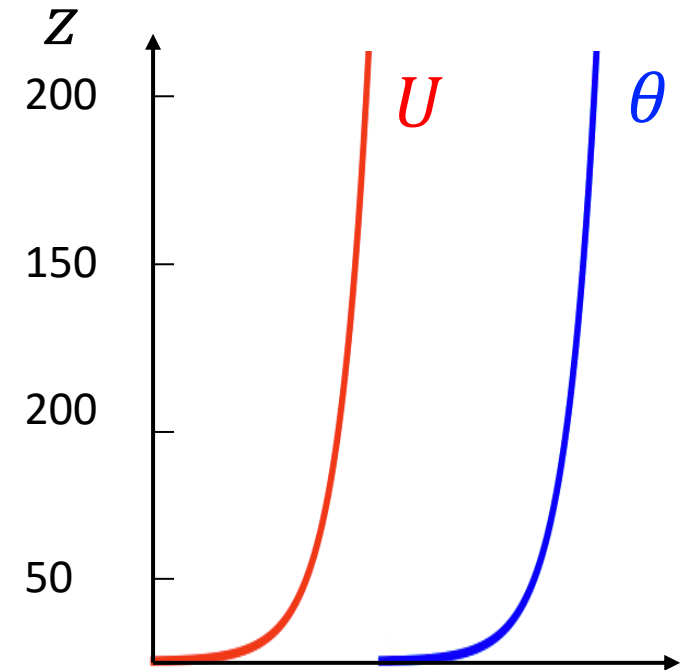
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Gives log profile for winds and potential temperature



‘Local’ turbulence closure at the surface – adding stability dependence

Adding stability dependence

Momentum

$$\kappa z \frac{\partial \bar{u}}{\partial z} = u_*$$

Integrate:

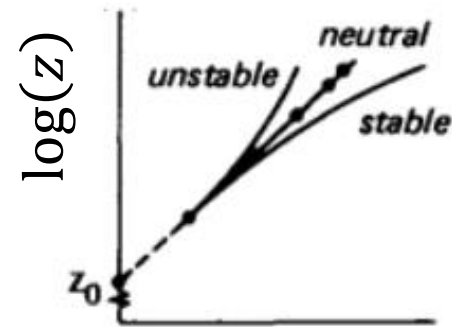
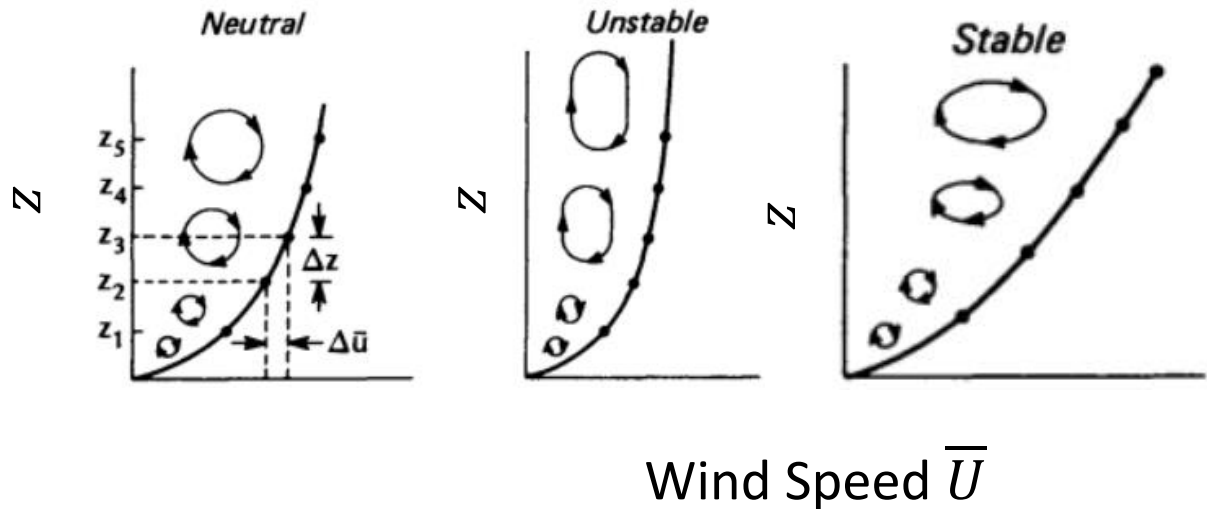
$$\bar{u}_z - \bar{u}_s = \frac{u_*}{\kappa} \log\left(\frac{z + z_0}{z_0}\right)$$

Thermodynamics

$$\kappa z \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

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Log profiles
are only valid
in neutral flow
conditions....

Adding stability dependence

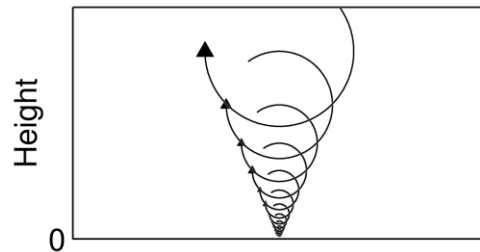
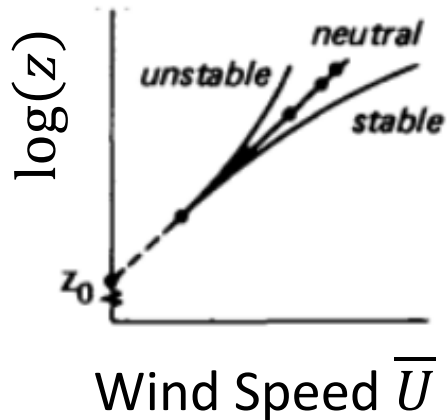
Momentum

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Neutral



Thermodynamics

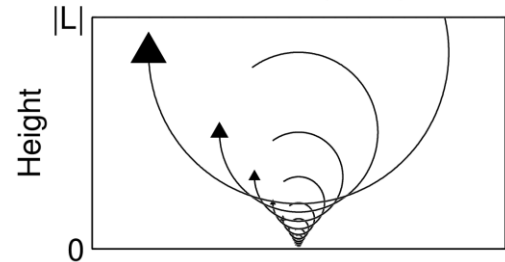
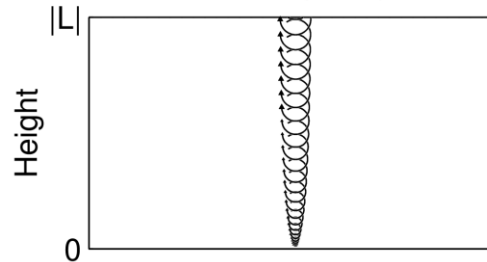
$$\kappa z \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \log\left(\frac{z + z_0}{z_0}\right)$$

Stable ($L > 0$)

Unstable ($L < 0$)



Mixing length modified to account for stability using a function ϕ :

$$l = \frac{\kappa z}{\phi(stability)}$$

This means we can get profiles of \bar{u} and $\bar{\theta}$ from flux

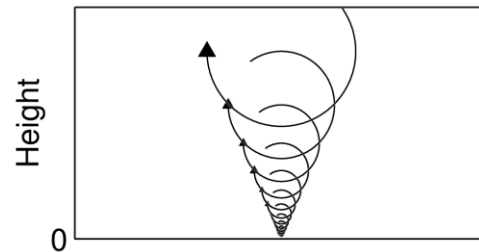
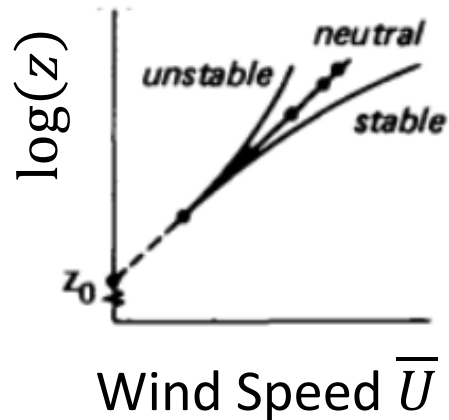
Momentum

$$\frac{\kappa z}{\phi_M} \frac{\partial \bar{u}}{\partial z} = u_*$$

Integrate:

$$\bar{u}_z - \bar{u}_s = \frac{u_*}{\kappa} \int_{z_0}^{z+z_0} \frac{1}{z} \phi_M dz$$

Neutral



Thermodynamics

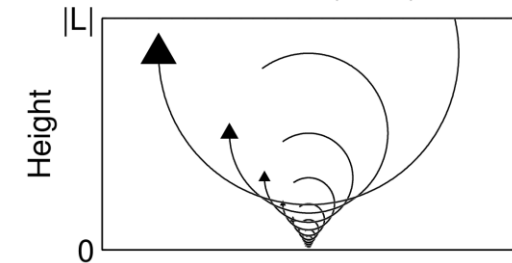
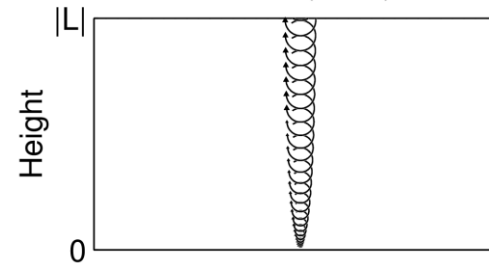
$$\frac{\kappa z}{\phi_H} \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \int_{z_0}^{z+z_0} \frac{1}{z} \phi_H dz$$

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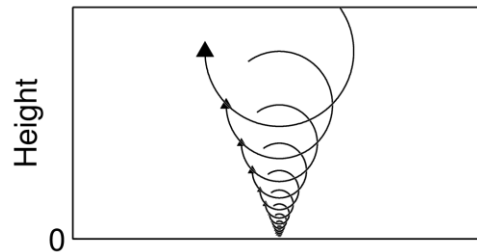
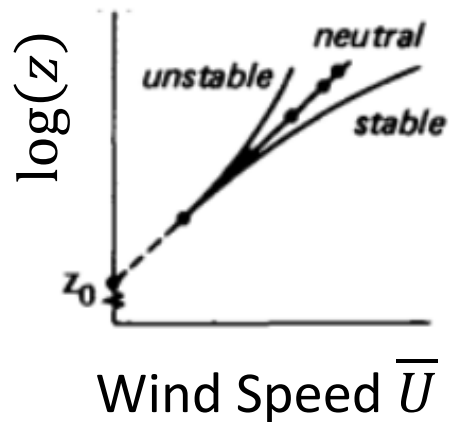
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Thermodynamics

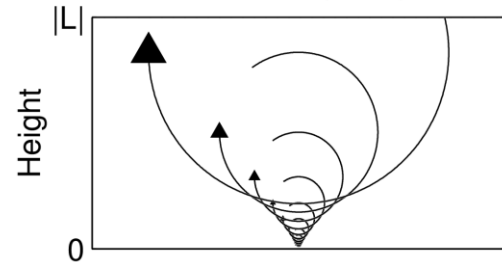
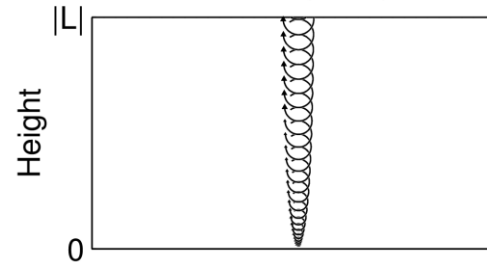
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Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \int_{z_0}^{z+z_0} \frac{1}{z} \phi_H dz$$

Stable ($L > 0$)

Unstable ($L < 0$)



Mixing length modified to account for stability using a function ϕ :

$$l = \frac{\kappa z}{\phi(\zeta)}, \quad \zeta = \frac{z}{L}$$

L = Obukhov length (will come back to this)

This means we can get profiles of \bar{u} and $\bar{\theta}$ from flux

Momentum

$$\frac{\kappa z}{\phi_M} \frac{\partial \bar{u}}{\partial z} = u_*$$

Integrate:

$$\bar{u}_z - \bar{u}_s = \frac{u_*}{\kappa} \int_{z_0}^{z+z_0} \frac{1}{z} \phi_M dz$$

Thermodynamics

$$\frac{\kappa z}{\phi_H} \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \int_{z_0}^{z+z_0} \frac{1}{z} \phi_H dz$$

Relationship between $\phi_M(\zeta)$, $\phi_H(\zeta)$
and ζ measured empirically and then
integrated vertically

To do this, requires a change of variable:

$$d\zeta = \frac{1}{L} dz$$

This means we can get profiles of \bar{u} and $\bar{\theta}$ from flux

Momentum

$$\frac{\kappa z}{\phi_M} \frac{\partial \bar{u}}{\partial z} = u_*$$

Integrate:

$$\bar{u}_z - \bar{u}_s = \frac{u_*}{\kappa} \int_{\zeta(z_0)}^{\zeta(z+z_0)} \frac{1}{\zeta} \phi_M(\zeta) d\zeta$$

Thermodynamics

$$\frac{\kappa z}{\phi_H} \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \int_{\zeta(z_0)}^{\zeta(z+z_0)} \frac{1}{\zeta} \phi_H(\zeta) d\zeta$$

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Integrate:

$$\bar{u}_z = \frac{u_*}{\kappa} \left[\log \left(\frac{z + z_{0m}}{z_{0m}} \right) - \Psi_M \left(\frac{z + z_{0m}}{L} \right) \right]$$

Thermodynamics

$$\frac{\kappa z}{\phi_H} \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \left[\log \left(\frac{z + z_{0m}}{z_{0H}} \right) - \Psi_H \left(\frac{z + z_{0M}}{L} \right) \right]$$

Relationship between $\phi_M(\zeta)$, $\phi_H(\zeta)$
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Ψ_H , Ψ_M are integrals of $\phi_M(\zeta)$

What is the Obukhov-length?

- Derived from scaling arguments - Reduces degrees of freedom so that 'universal' relations (they work for all situations) can be derived

$\zeta > 0$ Stable

$\zeta < 0$ Unstable

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buoyant production > shear production of turbulence

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$$\text{Buoyancy production: } \frac{g}{\theta} \overline{\theta' w'} = \frac{g}{\theta} \theta_* u_*$$

÷

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$$\div$$

$$\text{Shear production: } -\overline{u' w'} \frac{\partial u}{\partial z} = u_*^2 \frac{\partial u}{\partial z}$$

$$\zeta = \frac{z}{L} = \frac{g}{\theta} \frac{\theta_* u_*}{u_*^2 \frac{\partial u}{\partial z}} = -\frac{\frac{g}{\theta} \theta_* \kappa z}{u_*^2}$$

$$\text{Made use of: } \frac{\partial u}{\partial z} = \frac{u_*}{\kappa z}$$

This means we can get profiles of \bar{u} and $\bar{\theta}$ from flux

Momentum

$$\frac{\kappa z}{\phi_M} \frac{\partial \bar{u}}{\partial z} = u_*$$

Integrate:

$$\bar{u}_z = \frac{u_*}{\kappa} \left[\log \left(\frac{z + z_{0m}}{z_{0m}} \right) - \Psi_M \left(\frac{z + z_{0m}}{L} \right) \right]$$

Thermodynamics

$$\frac{\kappa z}{\phi_H} \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \left[\log \left(\frac{z + z_{0m}}{z_{0H}} \right) - \Psi_H \left(\frac{z + z_{0M}}{L} \right) \right]$$

Recall that:

$$\overline{u'w'} = u_*^2$$

$$\overline{\theta'w'} = \theta_* u_*$$

Relationship between $\phi_M(\zeta)$, $\phi_H(\zeta)$
and ζ measured empirically and then
integrated vertically

Ψ_H, Ψ_M are integrals of $\phi_M(\zeta)$

This means we can get surface fluxes

Momentum

$$\overline{\rho u'w'} = \rho u_*^2 = \rho C_M |\overline{u_z}|^2$$

Thermodynamics

$$\overline{\rho \theta'w'} = \rho u_* \theta_* = \rho C_H (\overline{\theta_z} - \overline{\theta_s}) |\overline{u_z}|$$

Surface exchange coefficient for heat:

$$C_H = \frac{\kappa^2}{\left[\log \left(\frac{z + z_{0m}}{z_{0m}} \right) - \Psi_M \left(\frac{z + z_{0m}}{L} \right) \right] \left[\log \left(\frac{z + z_{0m}}{z_{0H}} \right) - \Psi_H \left(\frac{z + z_{0m}}{L} \right) \right]}$$

Surface exchange coefficient for momentum:

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This means we can get surface fluxes **but...**

Momentum

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Thermodynamics

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Exchange coefficients depend on $\zeta = \frac{z+z_{0m}}{L}$, which itself depends on surface fluxes

How can we determine z/L and the surface fluxes?

1. Start with relationship between bulk Richardson number and z/L :

$$Ri_b = \frac{g}{\theta_z} \frac{(\overline{\theta_z} - \overline{\theta_s})z}{|\overline{u_z}|^2} = z \frac{g}{\theta_z} \frac{\theta_*}{u_*^2} \frac{C_M^{\frac{3}{2}}}{C_H} = \frac{z}{L} \frac{\left[\log\left(\frac{z+z_{0m}}{z_{0h}}\right) - \Psi_H\left(\frac{z+z_{0m}}{L}\right) \right]}{\left[\log\left(\frac{z+z_{0m}}{z_{0m}}\right) - \Psi_M\left(\frac{z+z_{0m}}{L}\right) \right]^2}$$

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2. Compute Ri_b from model fields and solve for $\frac{z}{L}$ by either:

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5. AND we can determine profiles of winds, temperature and humidity near the surface

Summary of Monin-Obukhov surface layer similarity theory

- The Obukhov-length is a measure of surface layer stability and can be thought of as the ratio of buoyancy / shear production of turbulence
- It is assumed that turbulent fluxes do not vary across the surface layer
- ‘Universal’ functions that relate the Obukhov length (stability) to the vertical profiles of conserved quantities (e.g. wind and temperature) in the surface layer can be derived from observations
- This is useful because we can relate Richardson number to z/L and get profiles and surface fluxes

What is the roughness length z_0 ?

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Momentum

$$\kappa z \frac{\partial \bar{u}}{\partial z} = u_*$$

Integrate:

$$\bar{u}_z - \bar{u}_s = \frac{u_*}{\kappa} \log \left(\frac{z + z_0}{z_0} \right)$$

Where $u_* = \sqrt{(u'w')_s} = \kappa z \left| \frac{\partial \bar{u}}{\partial z} \right|$ is the surface frictional velocity

θ_* is the temperature scaling, similarly, q_* is the moisture scaling

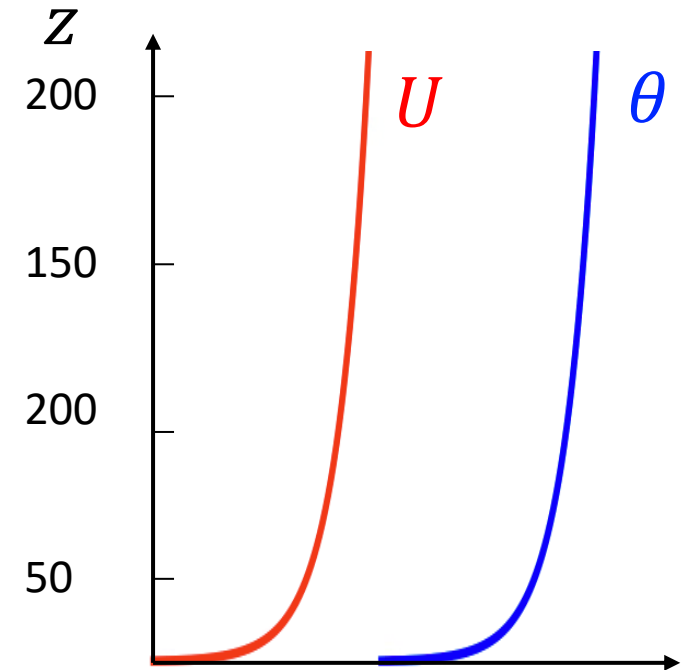
Thermodynamics

$$\kappa z \frac{\partial \bar{\theta}}{\partial z} = \theta_*$$

Integrate:

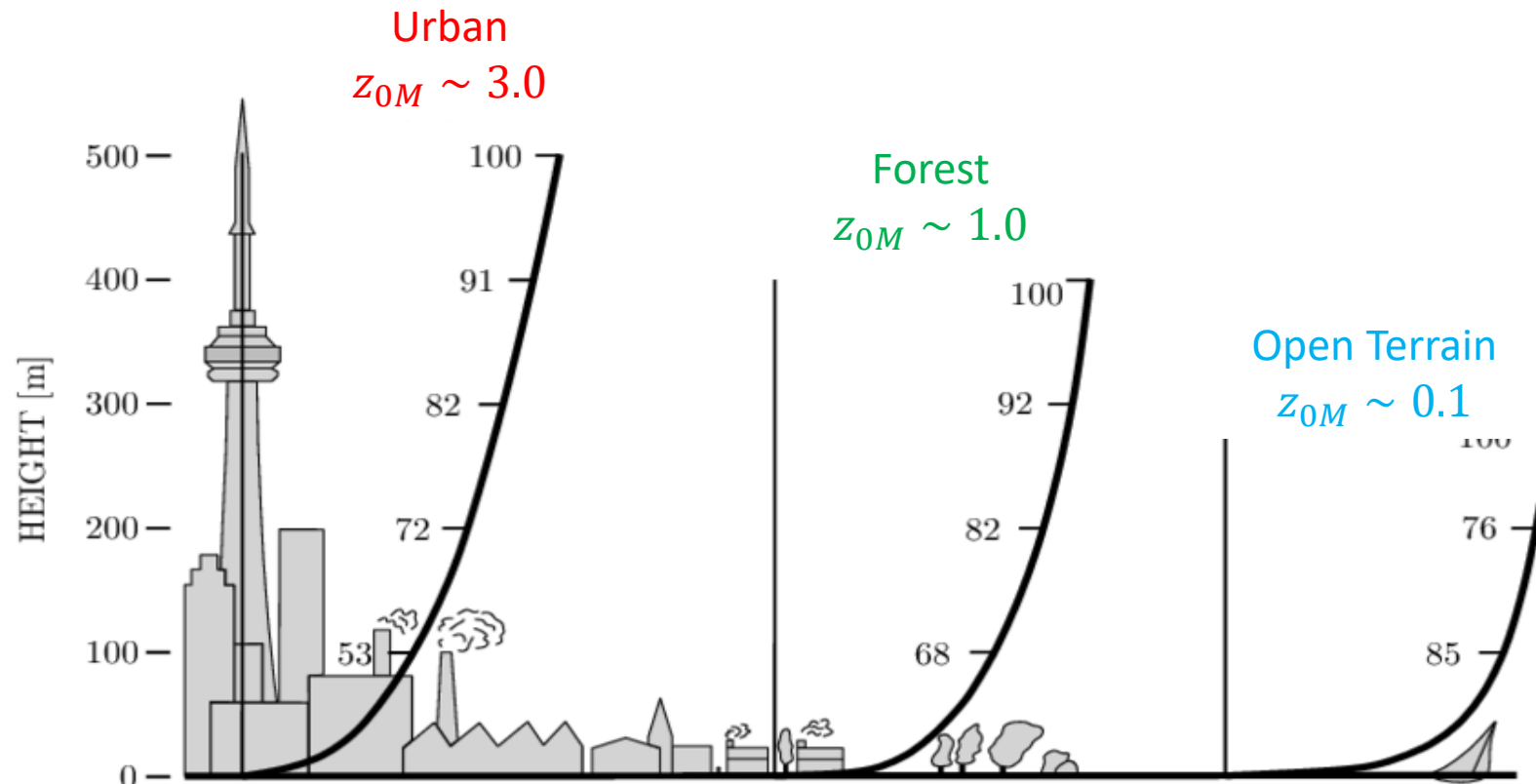
$$\bar{\theta}_z - \bar{\theta}_s = \frac{\theta_*}{\kappa} \log \left(\frac{z + z_0}{z_0} \right)$$

Gives log profile for winds and potential temperature



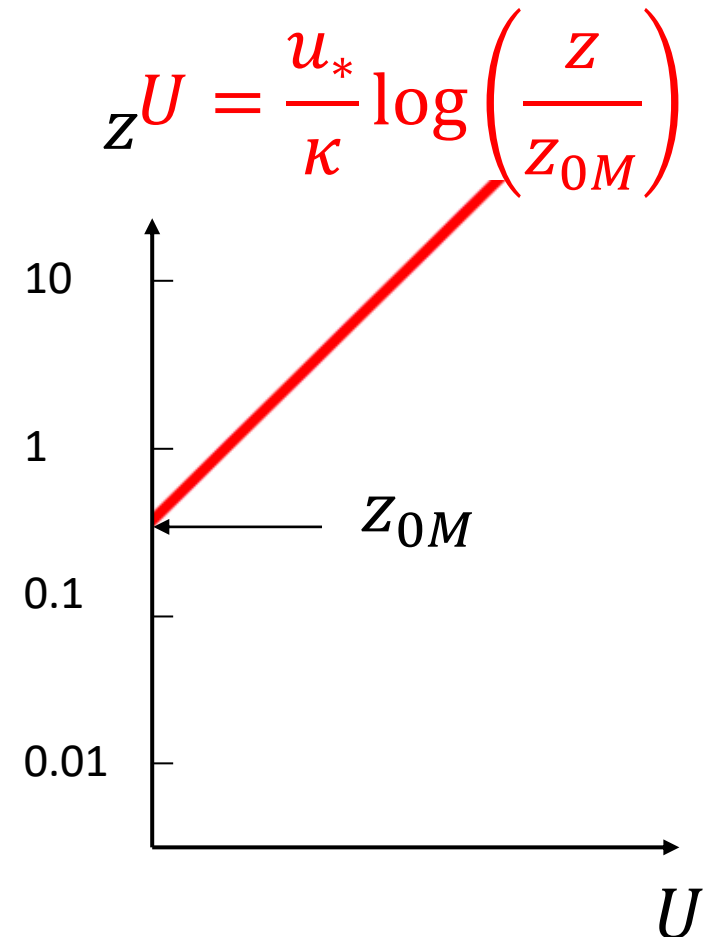
What is the roughness length z_0 ?

- Roughness length for momentum z_{0M} is not the same as for heat z_{0H}
- z_{0M} and z_{0H} determines the shape of the wind and temperature profiles
- They are a property of the underlying surface and are (assumed) to be a function of the height of the roughness elements



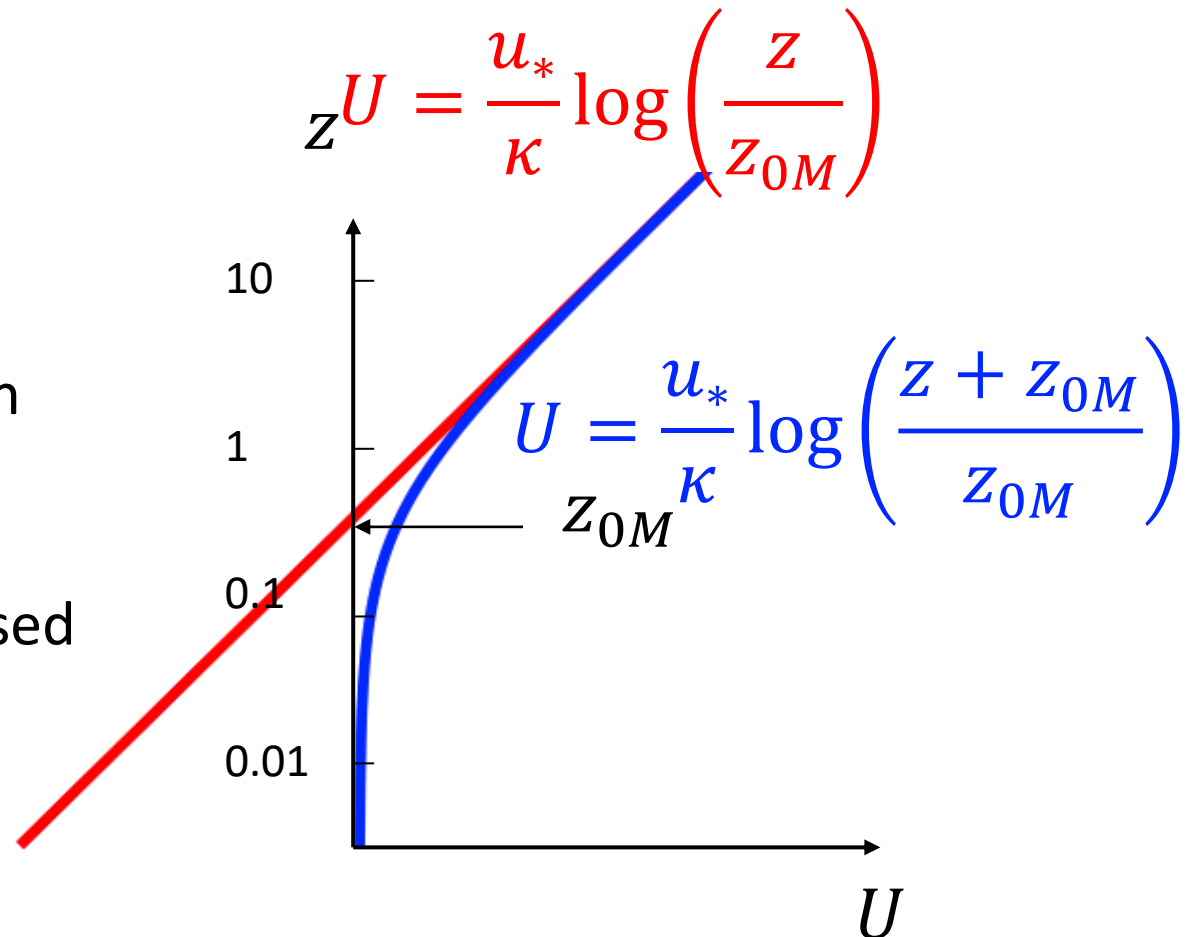
What is the roughness length z_0 ?

- Surface aerodynamic roughness length is defined from the logarithmic wind profile
- The roughness length is the height at which the winds become zero
- In the model, the displacement height is used to obtain $U = 0$ at $z = 0$. This



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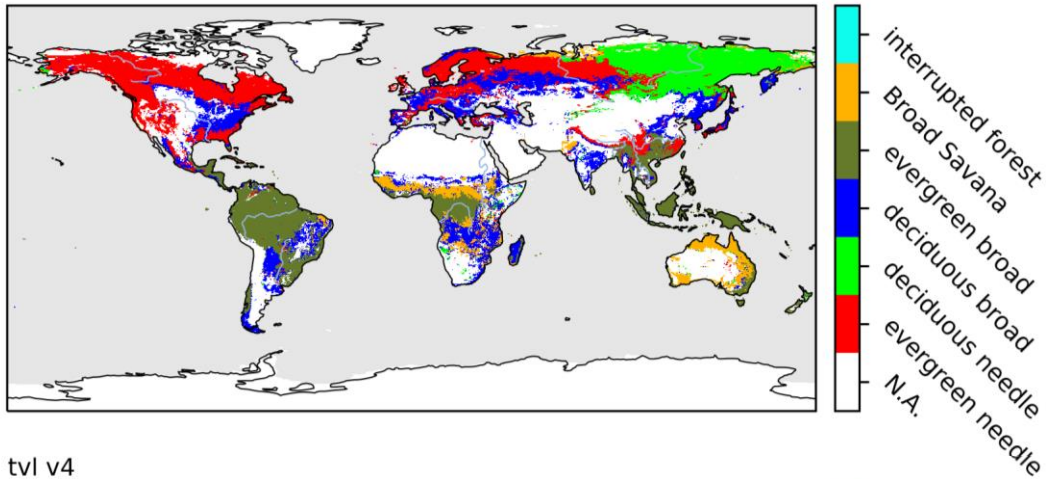


What is the roughness length z_0 over land?

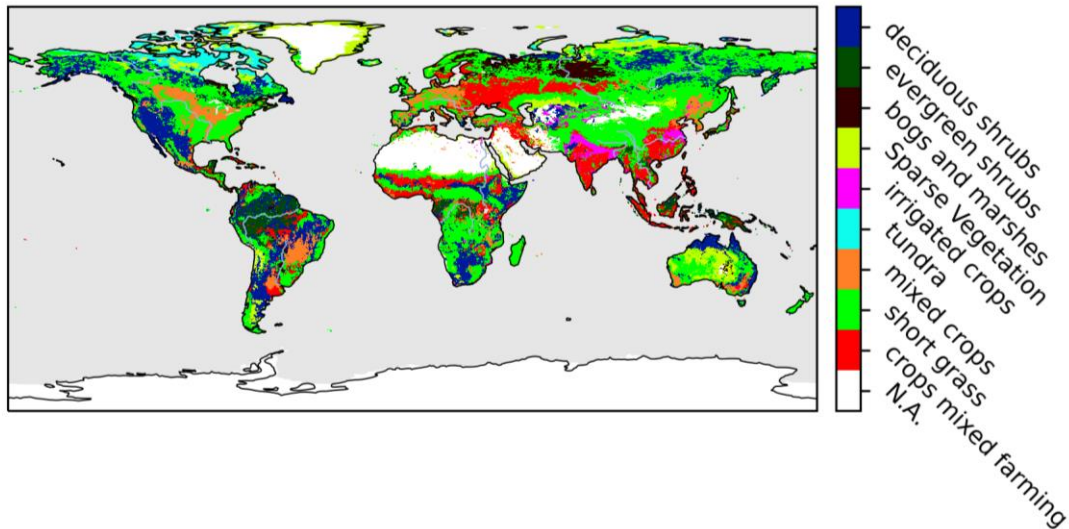
Note that $z_{0H} = \frac{z_{0M}}{10}$

Index	Vegetation type	H/L veg	z_{0m}	z_{0h}
1	Crops, mixed farming	L	0.25	$0.25 \cdot 10^{-2}$
2	Short grass	L	0.1	$0.1 \cdot 10^{-2}$
3	Evergreen needleleaf trees	H	2.0	2.0
4	Deciduous needleleaf trees	H	2.0	2.0
5	Deciduous broadleaf trees	H	2.0	2.0
6	Evergreen broadleaf trees	H	2.0	2.0
7	Tall grass	L	0.47	$0.47 \cdot 10^{-2}$
8	Desert	-	0.013	$0.013 \cdot 10^{-2}$
9	Tundra	L	0.034	$0.034 \cdot 10^{-2}$
10	Irrigated crops	L	0.5	$0.5 \cdot 10^{-2}$
11	Semidesert	L	0.17	$0.17 \cdot 10^{-2}$
12	Ice caps and glaciers	-	$1.3 \cdot 10^{-3}$	$1.3 \cdot 10^{-4}$
13	Bogs and marshes	L	0.5	$0.5 \cdot 10^{-2}$
14	Inland water	-	-	-
15	Ocean	-	-	-
16	Evergreen shrubs	L	0.100	$0.1 \cdot 10^{-2}$
17	Deciduous shrubs	L	0.25	$0.25 \cdot 10^{-2}$
18	Mixed forest/woodland	H	2.0	2.0
19	Interrupted forest	H	1.1	1.1
20	Water and land mixtures	L	-	-

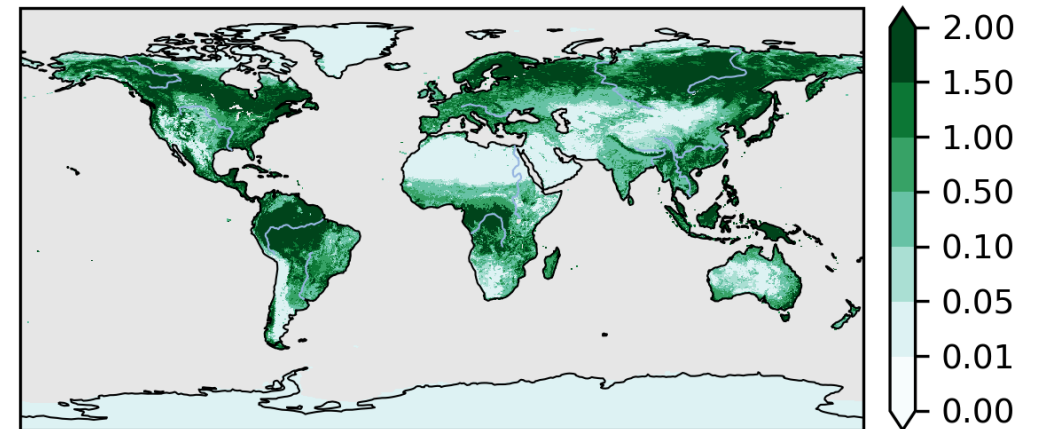
tvh v4



tvI v4



z0m None v4



What is the roughness length z_0 over ocean?

$$z_{0M} = \alpha_M \frac{\nu}{u_*} + \alpha_{ch} \frac{u_*^2}{g}$$

$$z_{0H} = \alpha_H \frac{\nu}{u_*}$$

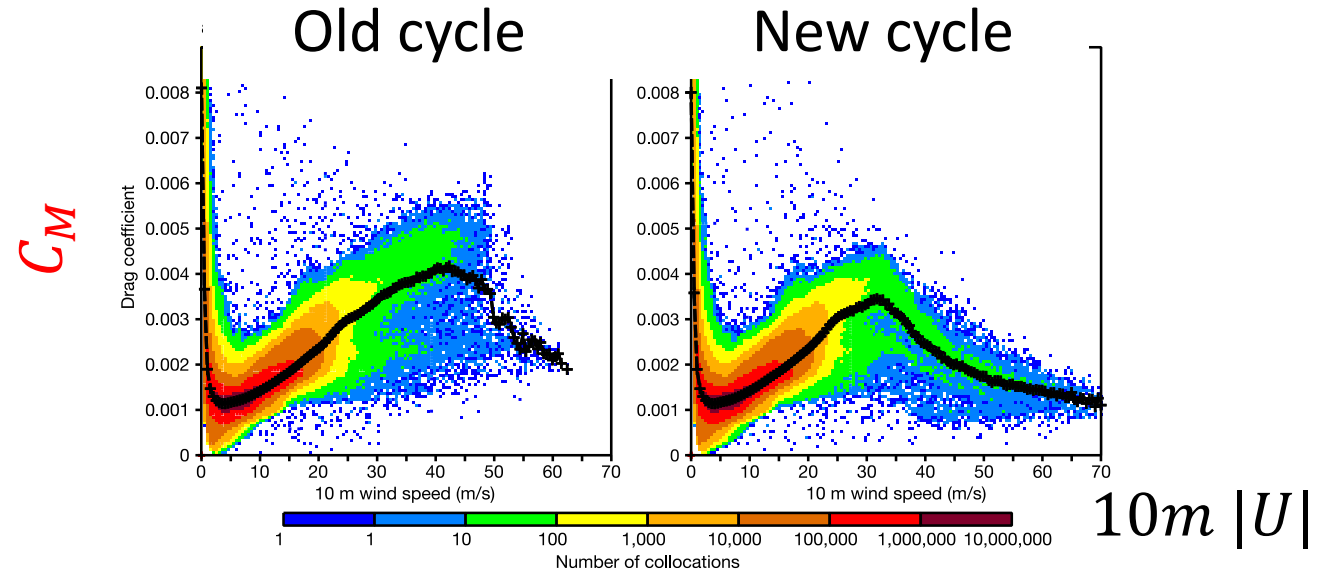
$$z_{0Q} = \alpha_Q \frac{\nu}{u_*}$$

ν = kinematic viscosity

$$u_* = C_M^{\frac{1}{2}} |U_n|$$

$\alpha_M, \alpha_H, \alpha_Q$ = constants

α_{ch} = Charnock coefficient,
provided by the wave model



$$C_M = \frac{\kappa^2}{\left[\log \left(\frac{z + z_{0m}}{z_{0m}} \right) - \Psi_M \left(\frac{z + z_{0m}}{L} \right) \right]^2}$$

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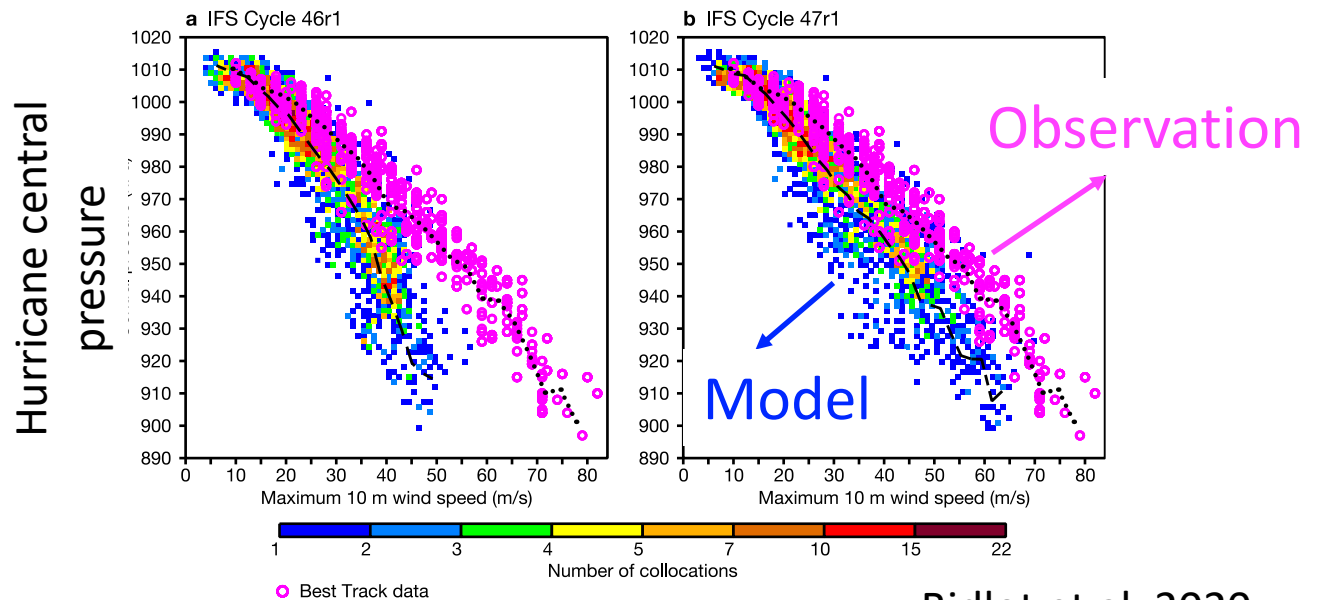
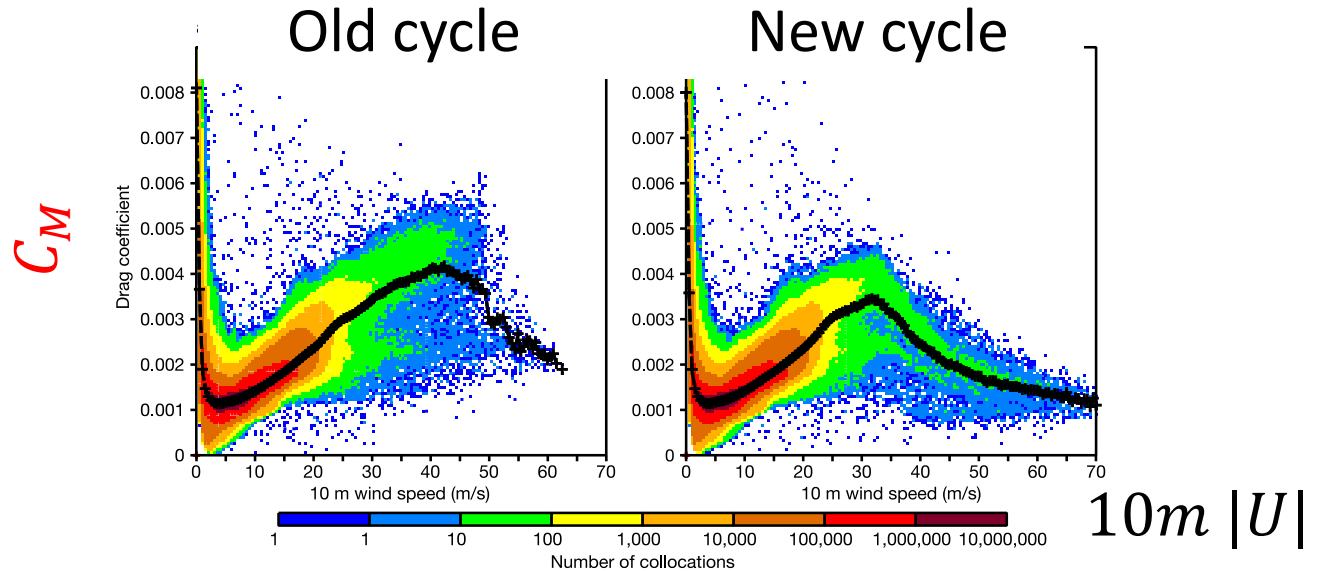
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What is the roughness length z_0 over sea-ice?

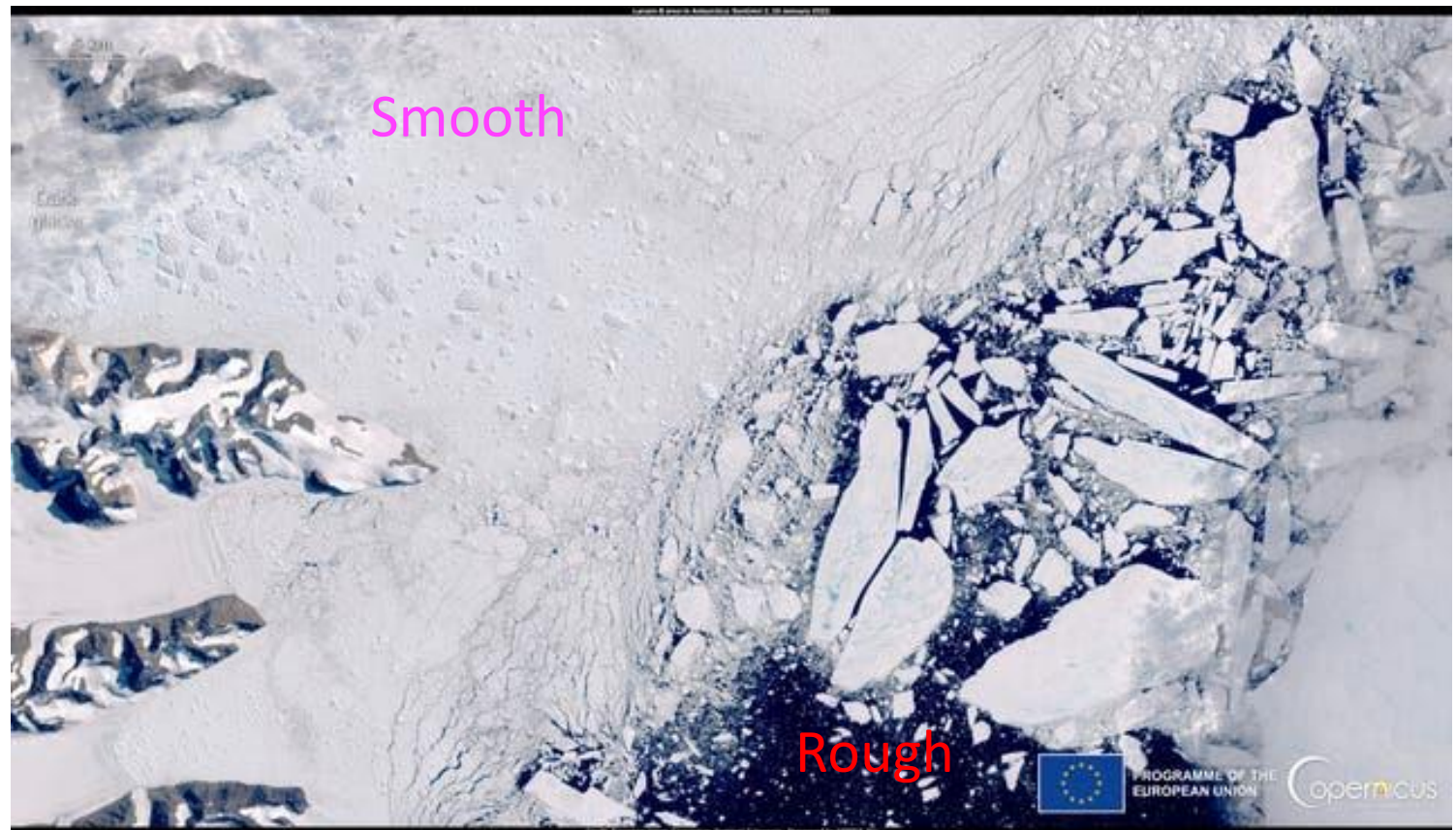
$$z_{0M} = \max(10^{-3}, f(c_i))$$

$$z_{0H} = 10^{-3}$$

$$z_{0Q} = 10^{-3}$$

c_i = sea ice concentration

$f(c_i)$: The dependence on sea-ice concentration reflects observation that partial ice-cover leads to more broken up sea ice and therefore increased drag



‘Local’ turbulence closure: eddy
diffusion above the surface

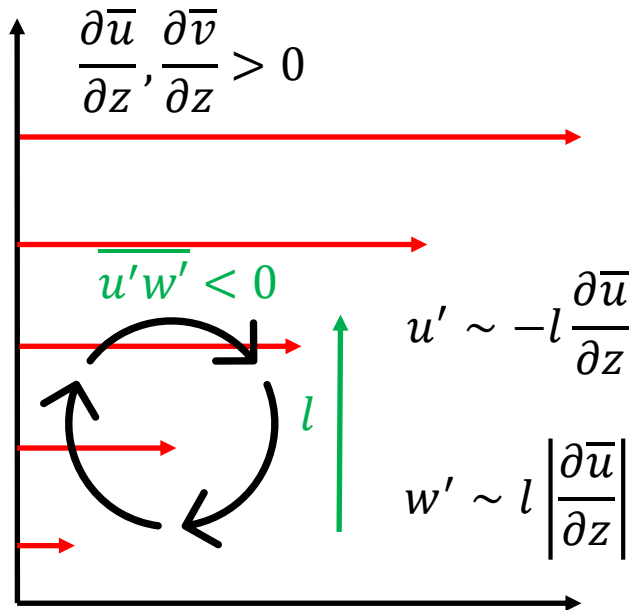
'Local' turbulence closure: eddy diffusion above the surface

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{u}}{\partial z}$$

Thermodynamics

$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| \frac{\partial \bar{\theta}}{\partial z}$$



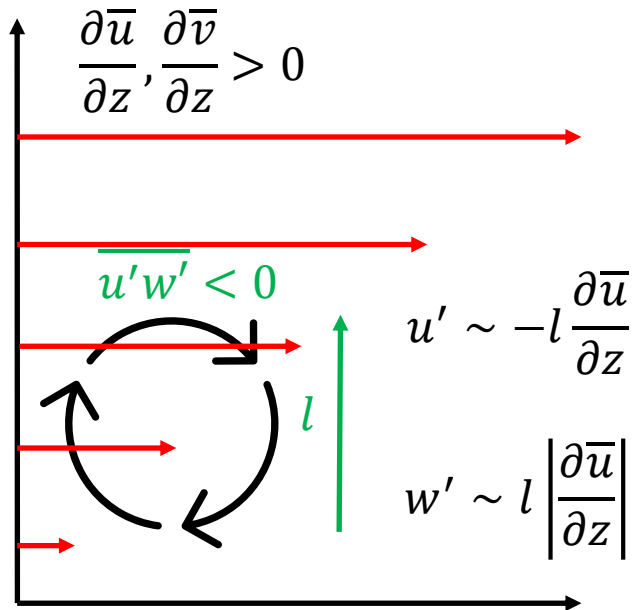
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Thermodynamics

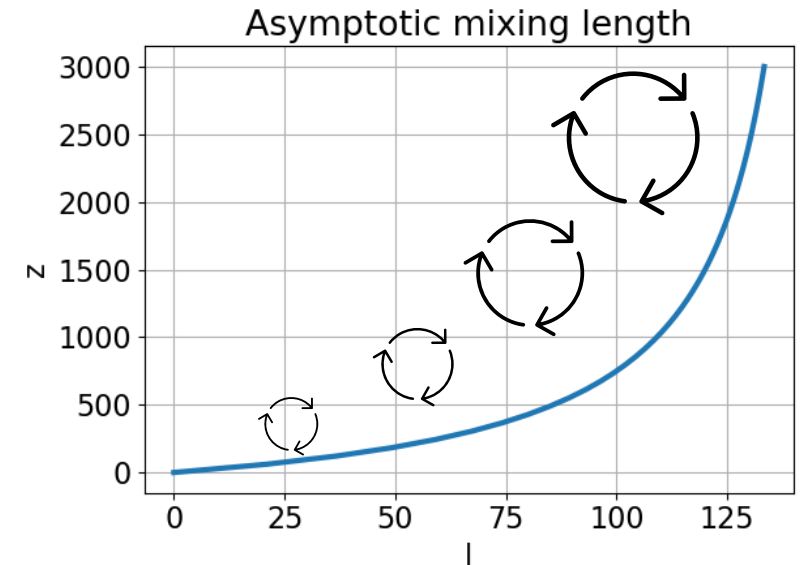
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Size of eddies get larger further away from the surface:

$$l \sim \frac{\kappa z \lambda}{\kappa z + \lambda}$$

κ = von-Karman constant
 λ = asymptotic mixing length (150 m)



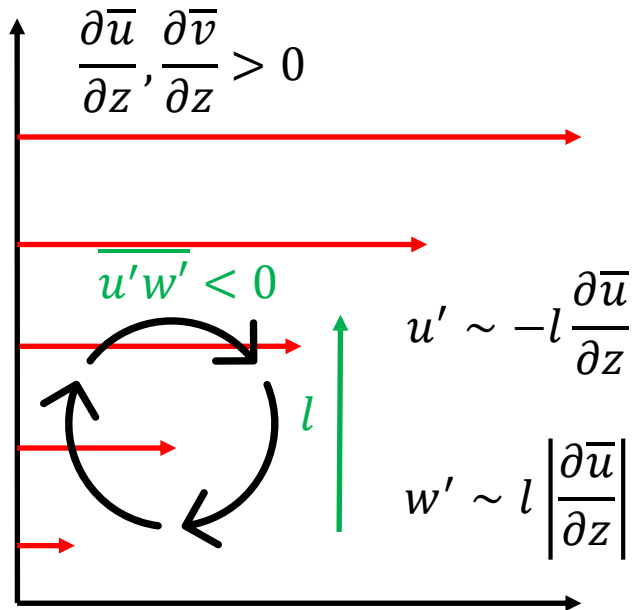
'Local' turbulence closure: eddy diffusion above the surface

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| f_M(Ri) \frac{\partial \bar{u}}{\partial z}$$

Thermodynamics

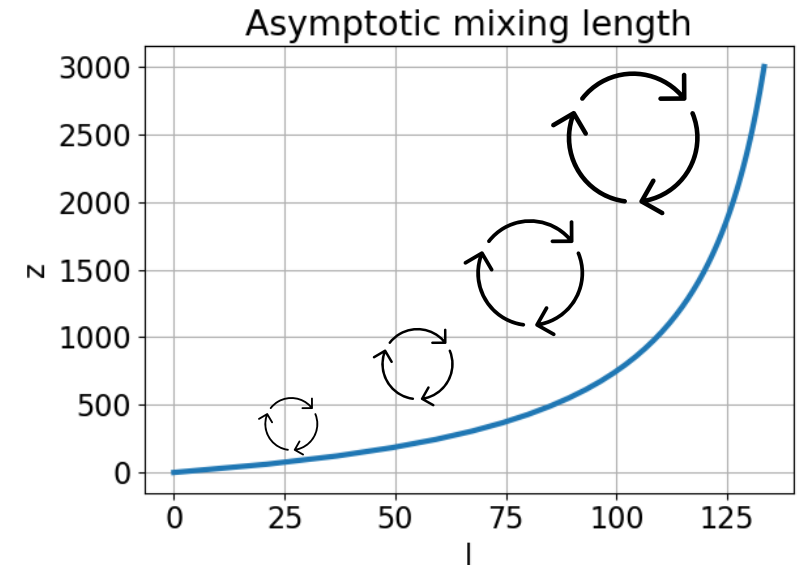
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$f_M(Ri), f_H(Ri)$ determined empirically and depend on $Ri(z)$, since we are away from the surface

Local similarity theory in the outer layer

Momentum

$$\overline{u'w'} \sim -K_M \frac{\partial \bar{u}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| f_M(Ri) \frac{\partial \bar{u}}{\partial z}$$

Thermodynamics

$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| f_H(Ri) \frac{\partial \bar{\theta}}{\partial z}$$

- In stable conditions, the mid and upper boundary layer may not be in equilibrium with the surface fluxes
- Local fluxes and stability (Ri) dominate

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- In stable conditions, the mid and upper boundary layer may not be in equilibrium with the surface fluxes
- Local fluxes and stability (Ri) dominate
- Local similarity states that the surface layer functions can be used in the outer layer:

$$K_H = \frac{l^2}{\phi_H(\zeta)\phi_M(\zeta)} \left| \frac{\partial \bar{u}}{\partial z} \right|$$

$$K_M = \frac{l^2}{\phi_M^2(\zeta)} \left| \frac{\partial \bar{u}}{\partial z} \right|$$

Thermodynamics

$$\overline{\theta'w'} \sim -K_H \frac{\partial \bar{\theta}}{\partial z} = -l^2 \left| \frac{\partial \bar{u}}{\partial z} \right| f_H(Ri) \frac{\partial \bar{\theta}}{\partial z}$$

Use the relation

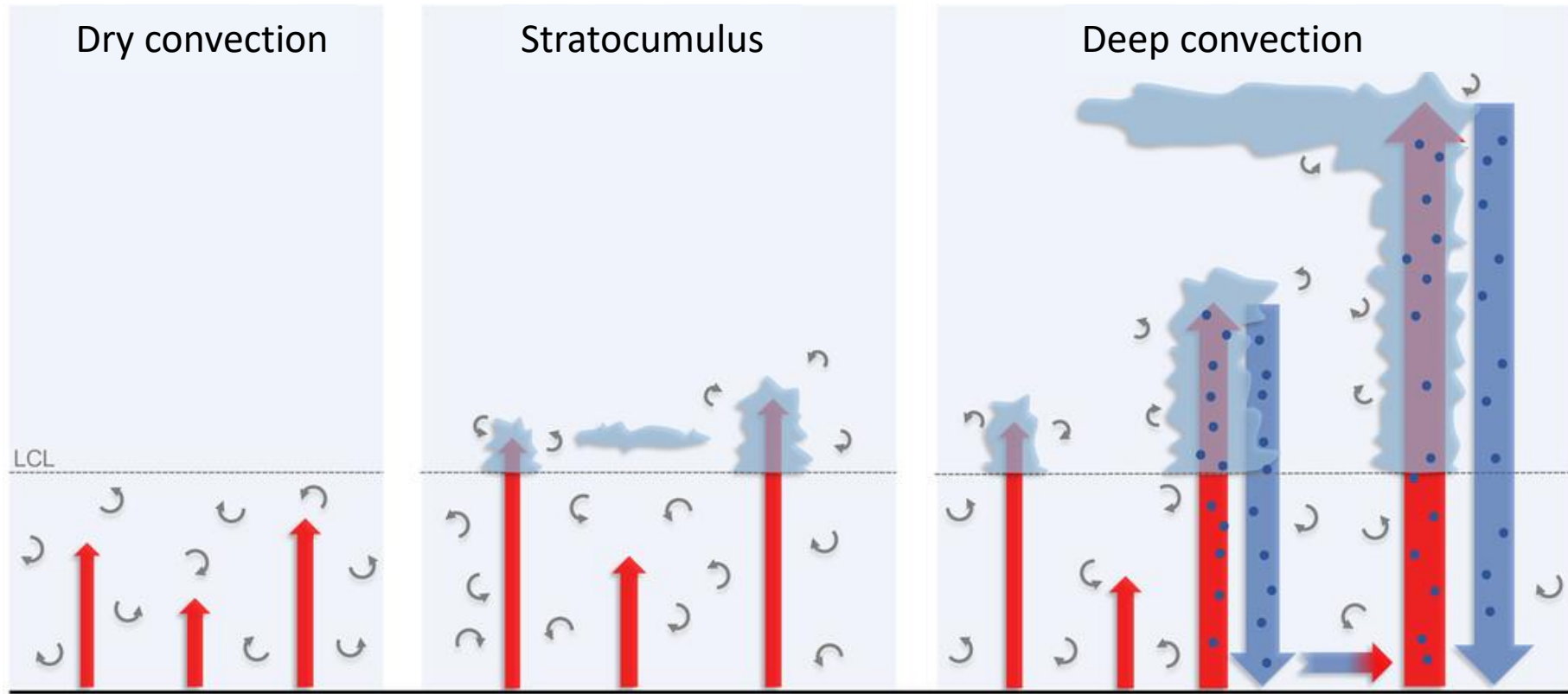
$$Ri = \zeta \frac{\phi_H(\zeta)}{\phi_M^2(\zeta)}$$

to convert $\zeta = \frac{z}{L}$ to the gradient Richardson number in the outer layer

‘Non-Local’ turbulence: eddy-diffusivity mass-flux (EDMF)

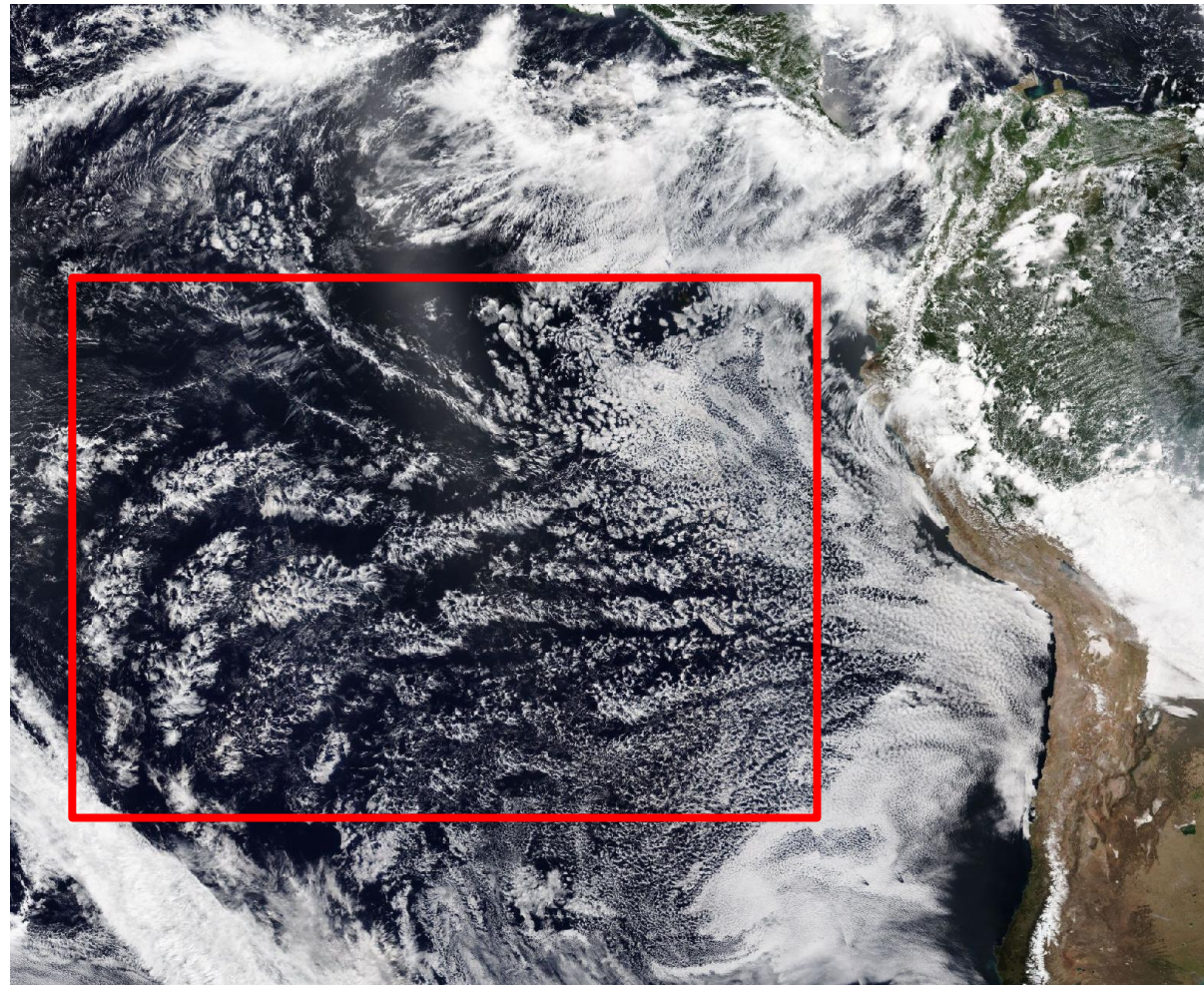
'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

Local turbulent diffusion fails in convective boundary layers because it yields unrealistic zero flux in an environment with small gradients



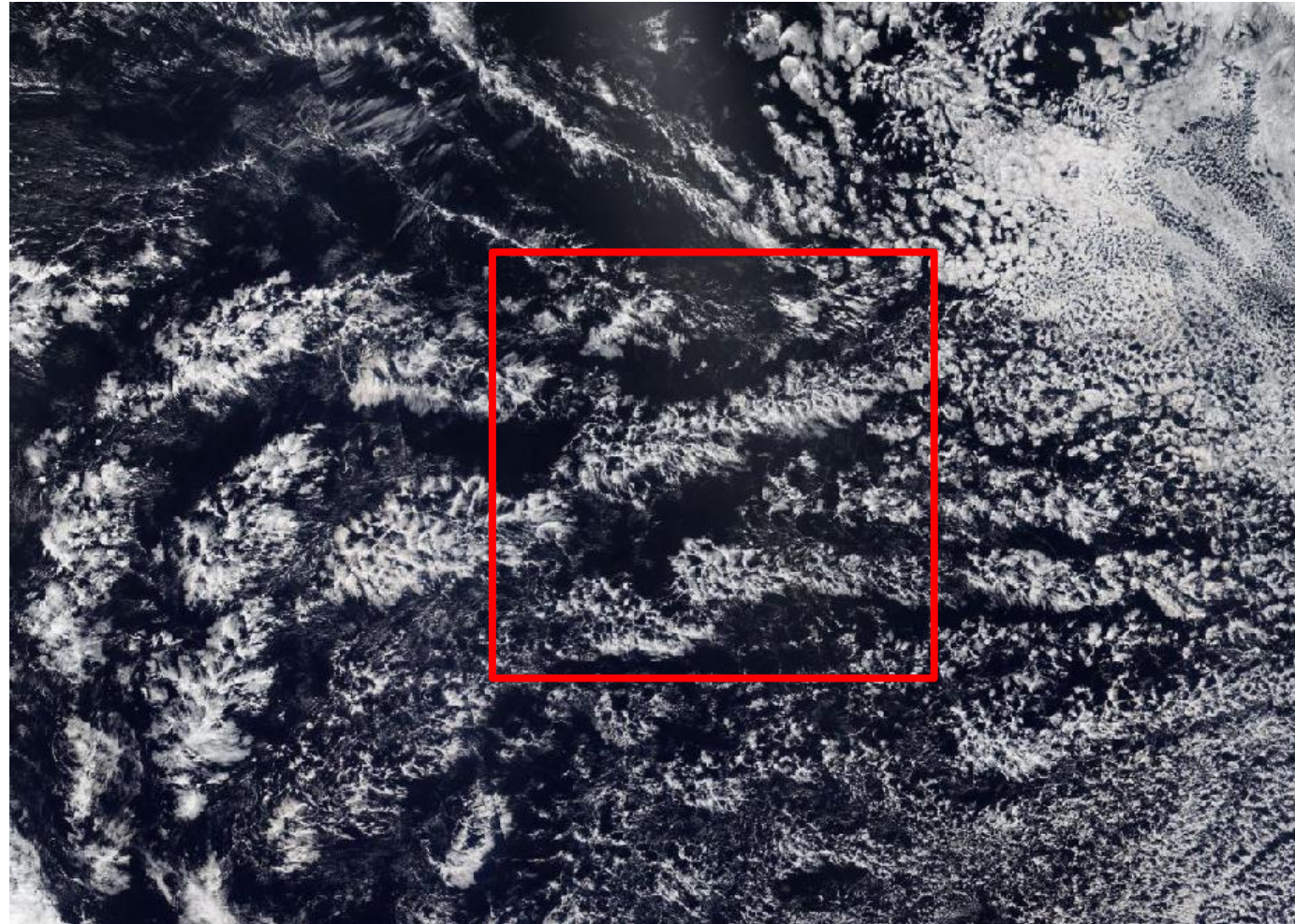
'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

In convective boundary layers, the area of strongest updraft is typically much smaller than the environment



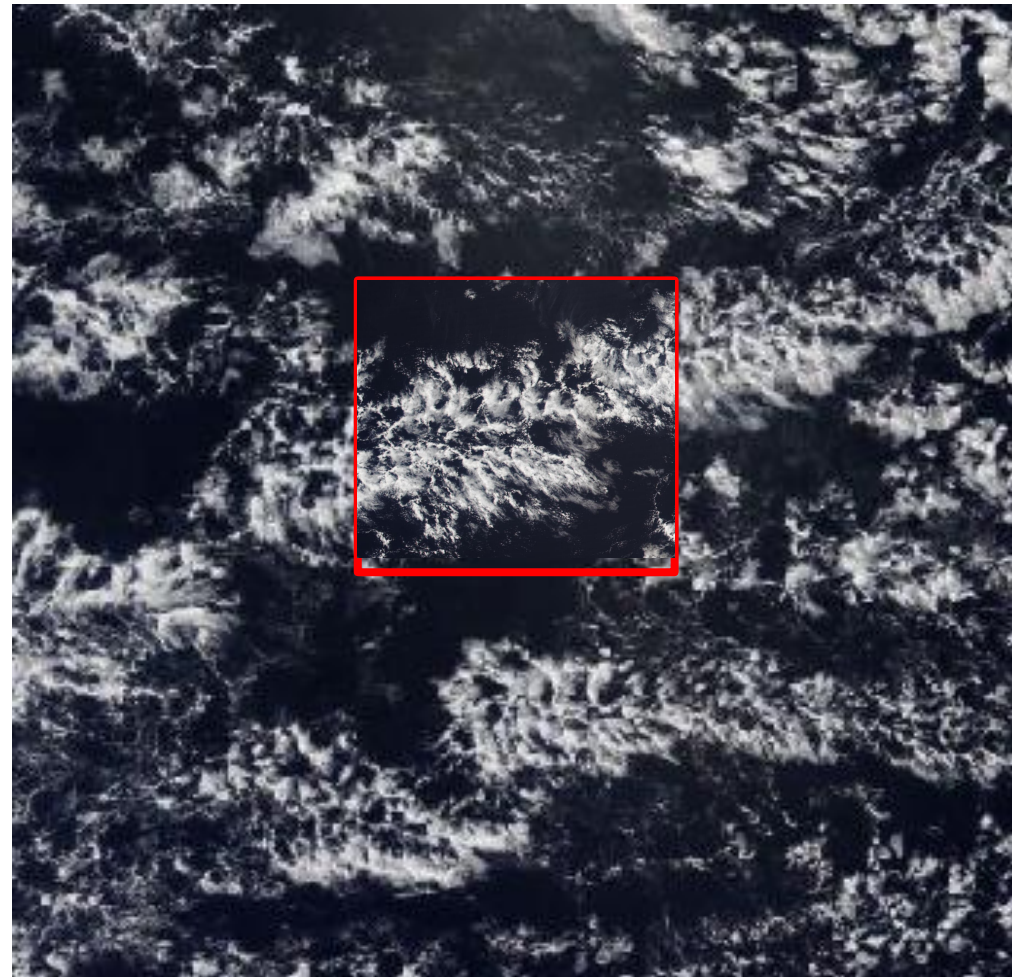
'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

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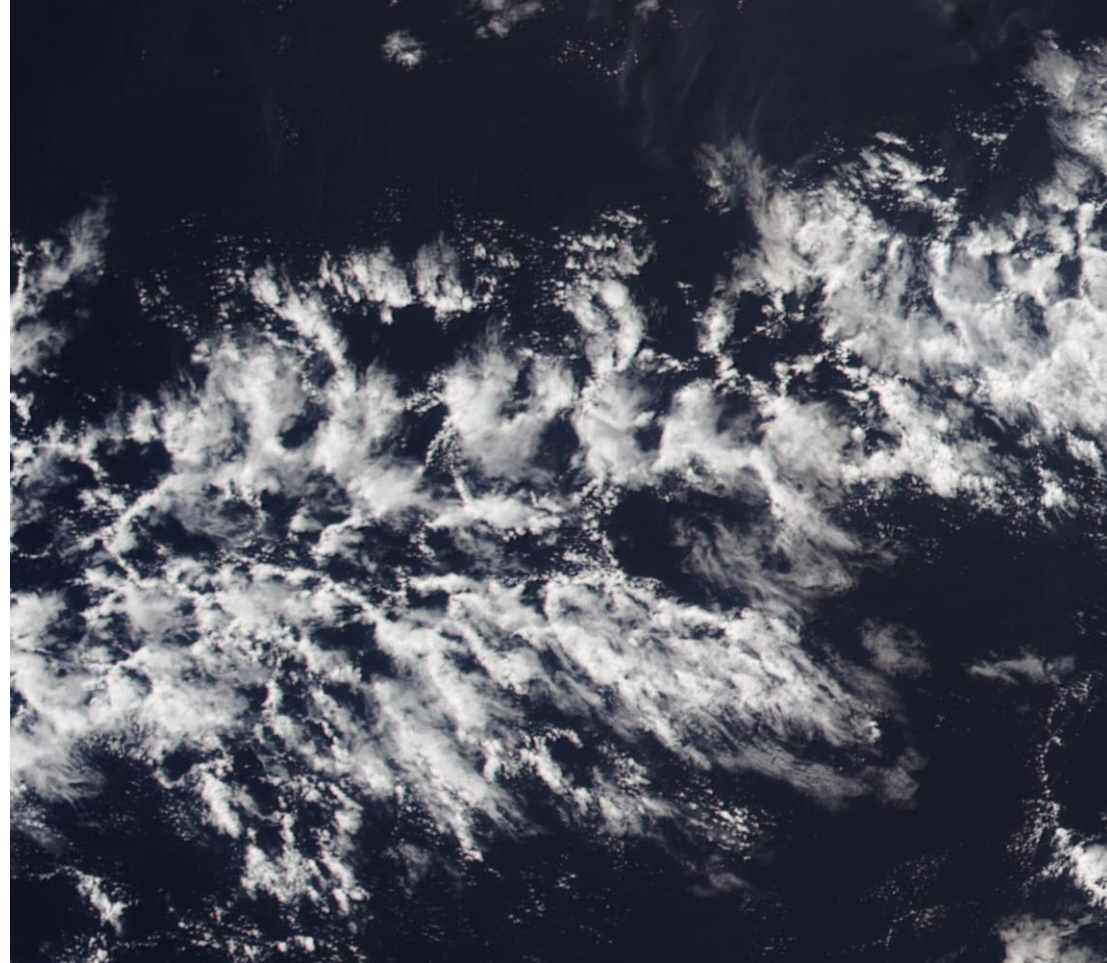
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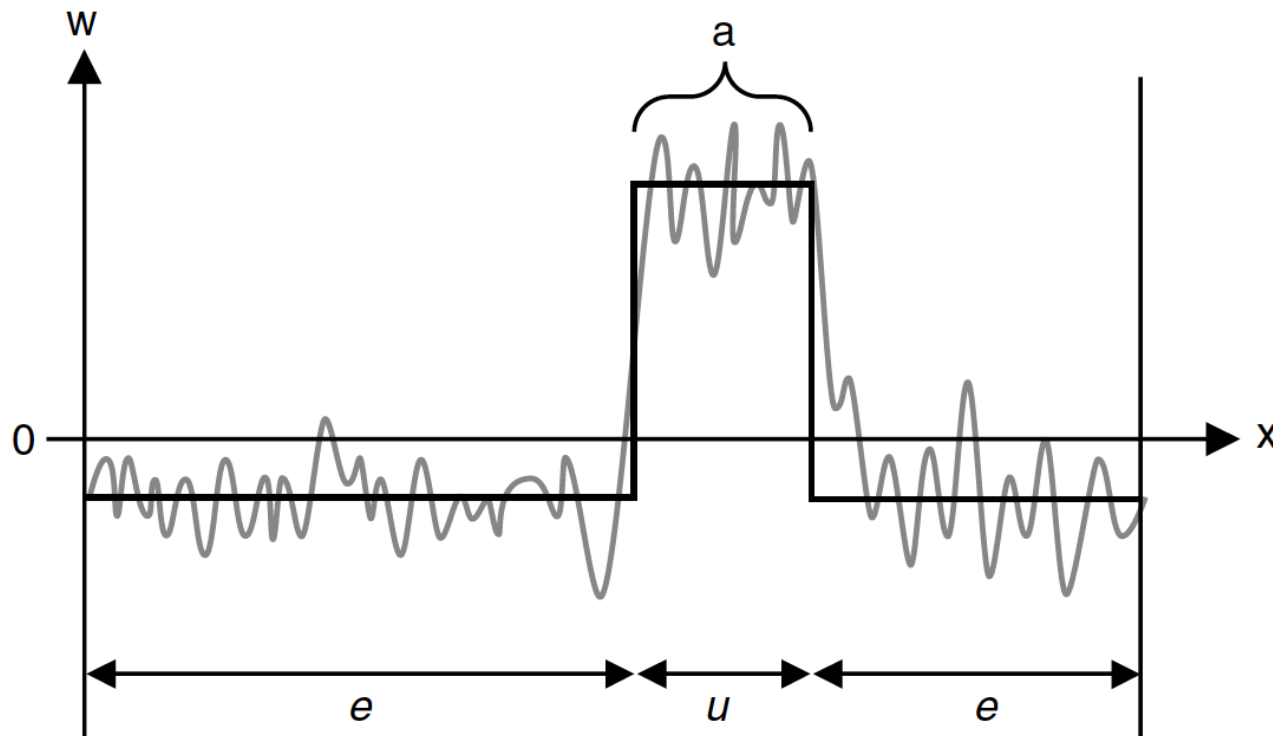
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'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

Total turbulent flux of ϕ :

$$\overline{\phi'w'} = a\overline{\phi'_u w'} + (1 - a)\overline{\phi'_e w'} + a(\overline{w}^u - \overline{w})(\overline{\phi}^u - \overline{\phi}^e)$$



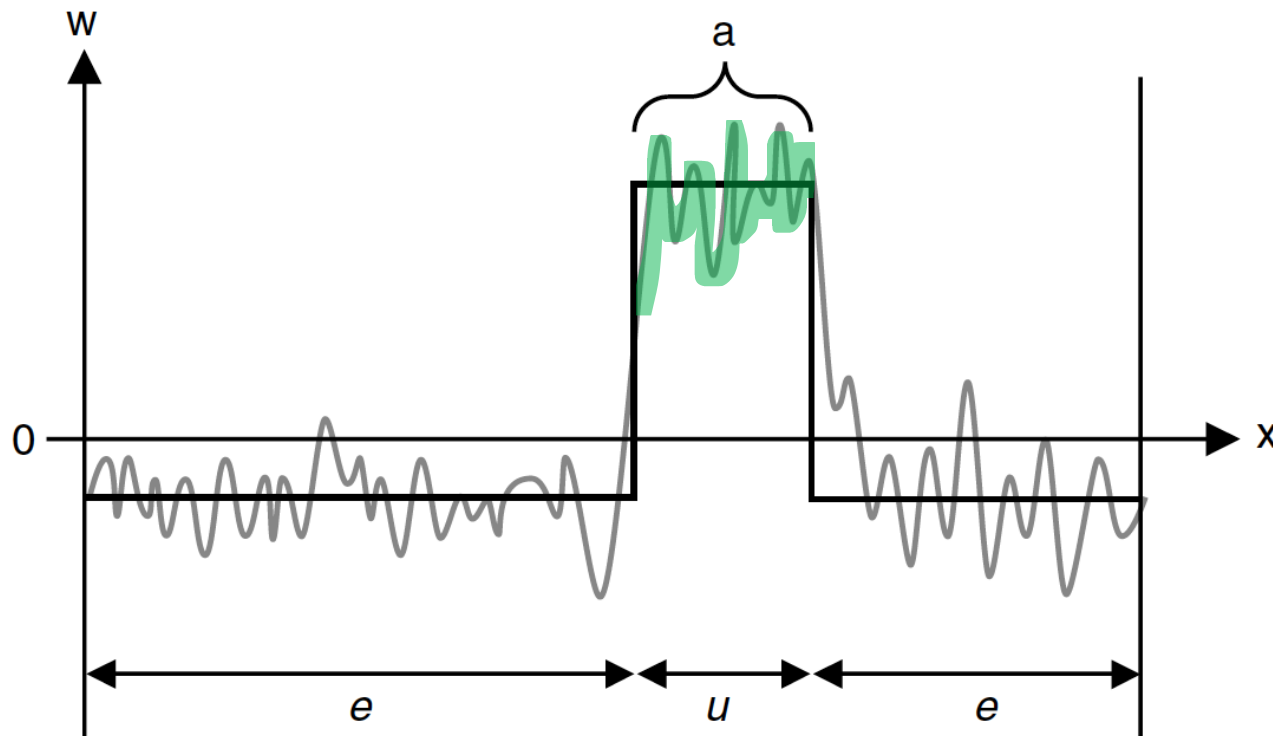
Turbulent flux within
the strong updraft
region

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Subcore
flux



Turbulent flux within
the strong updraft
region

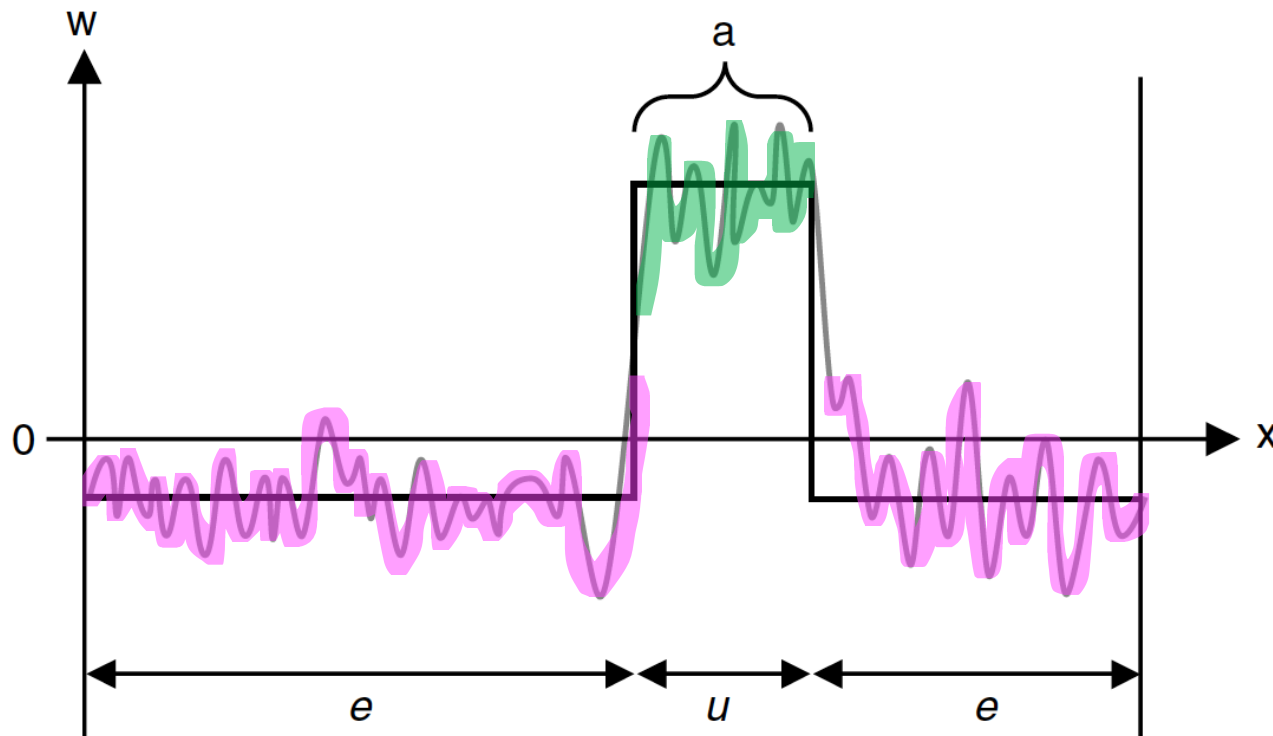
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Subcore
flux

Environmental
flux



Turbulent flux in the environment outside the strongest updraft

'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

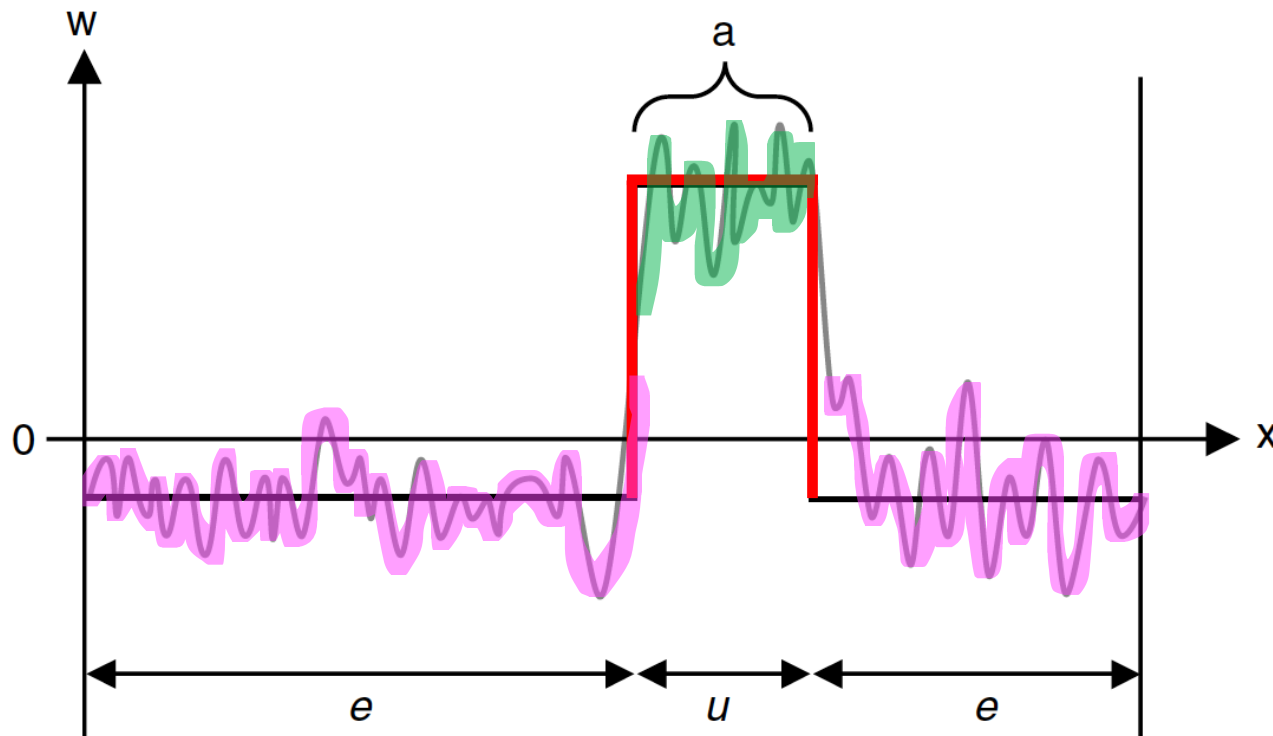
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Subcore
flux

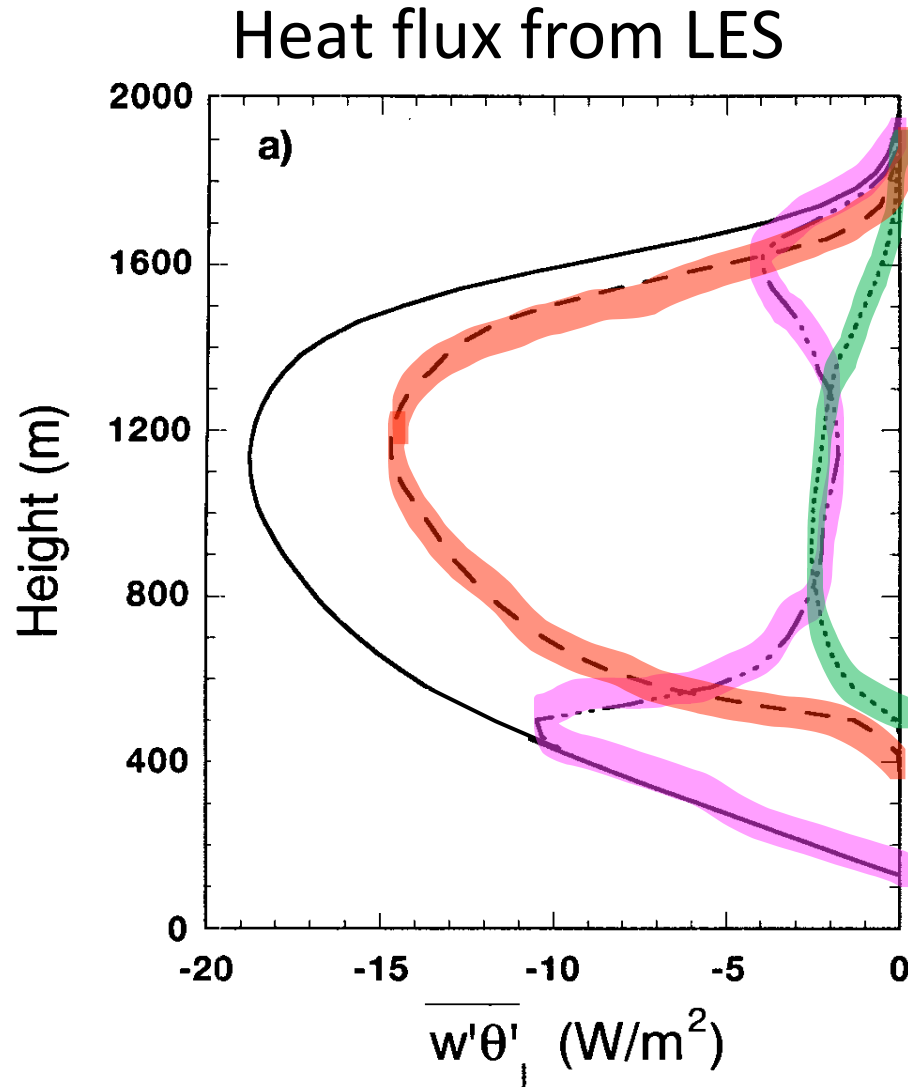
Environmental
flux

Mass
flux



Mean flux inside the
strongest updraft
region

'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)



Total turbulent flux of ϕ :

$$\overline{\phi'w'} = a\overline{\phi'_u w'} +$$

$$(1 - a)\overline{\phi'_e w'} +$$

$$a(\overline{w^u} - \overline{w})(\overline{\phi^u} - \overline{\phi^e})$$

Subcore
flux

Environmental
flux

Mass
flux

M-flux covers 80% of the flux for
heat and moisture,

Siebesma & Cuijpers, 1995

less for momentum – environment plays a bigger
role for momentum transport

Zhu 2015, Schlemmer et al, 2016

'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

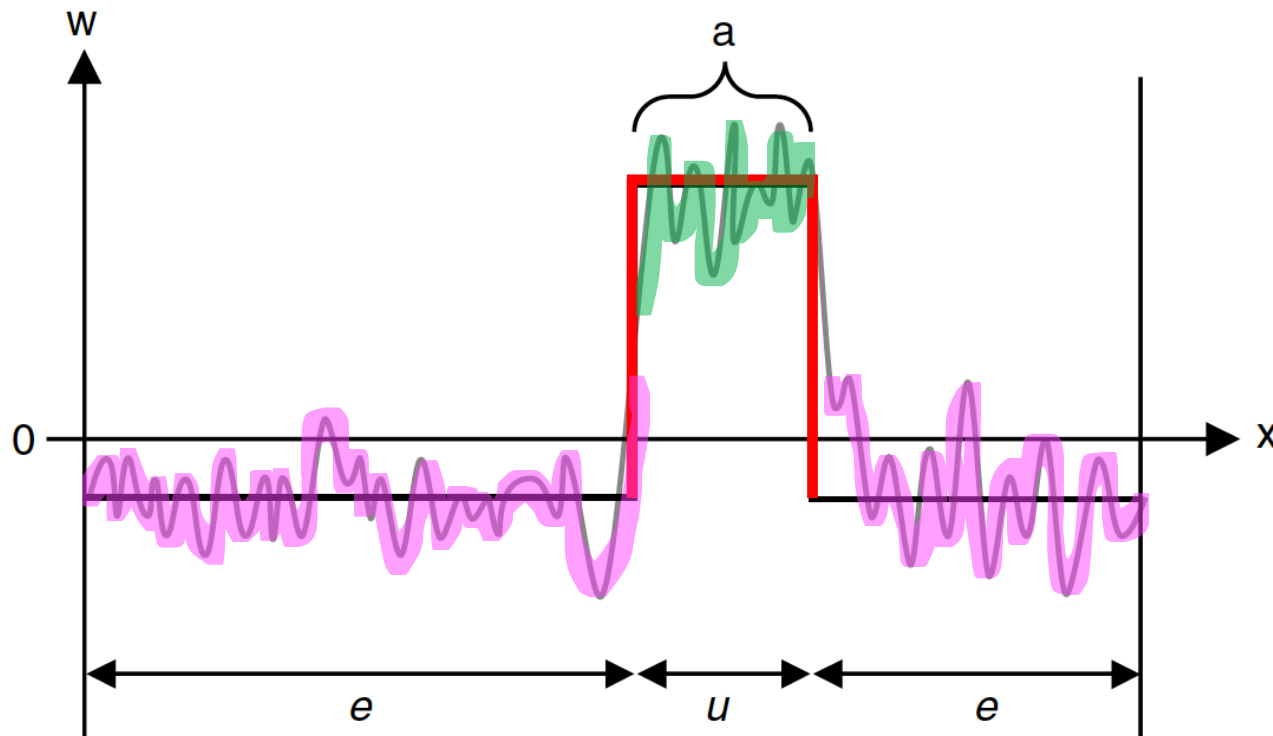
Total turbulent flux of ϕ :

$$\overline{\phi'w'} = \overbrace{a\phi'_u w'}^{\text{Subcore flux}} + \overbrace{(1-a)\phi'_e w'}^{\text{Environmental flux}} + \overbrace{a(\overline{w}^u - \overline{w})(\overline{\phi}^u - \overline{\phi}^e)}^{\text{Mass flux}}$$

Subcore
flux

Environmental
flux

Mass
flux



Assumptions made:

1. Area of strongest updraft is small compared with the environment ($a \ll 1$).

Subcore flux is neglected

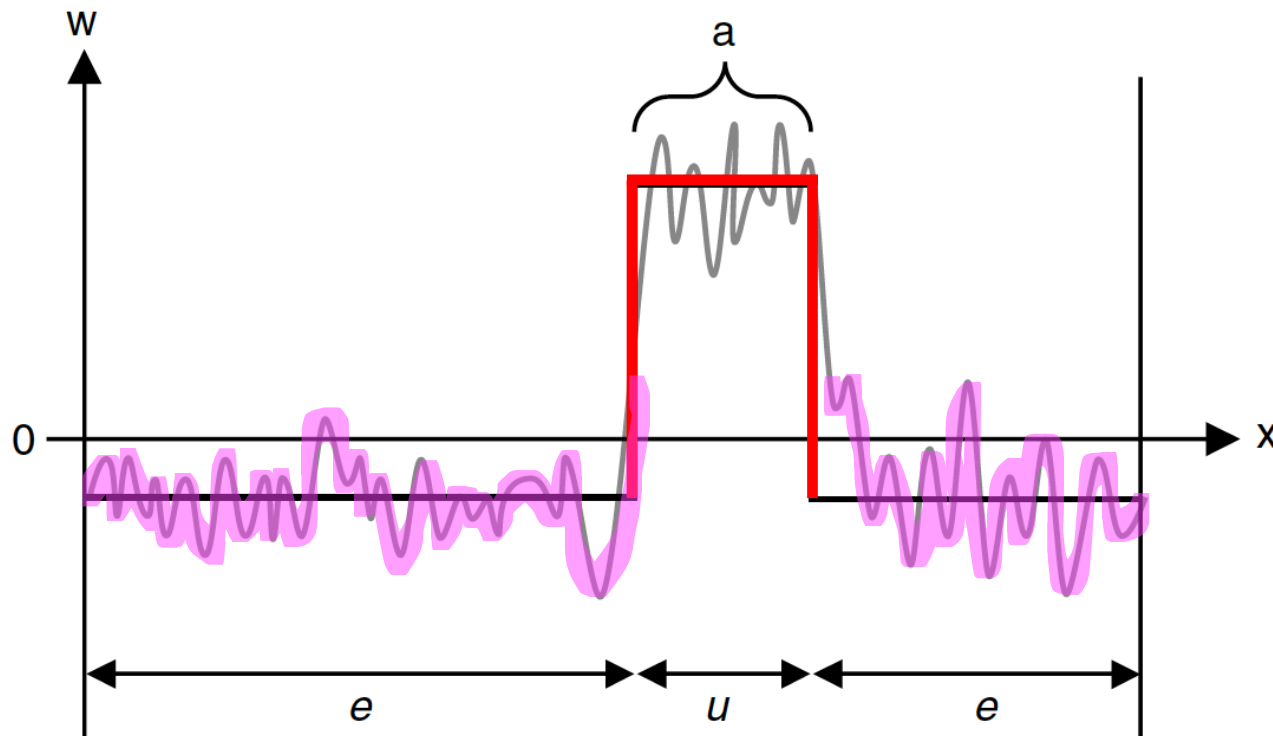
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$$\overline{\phi'w'} = (1 - a)\overline{\phi_e'w'} + a(\overline{w}^u - \overline{w})(\overline{\phi}^u - \overline{\phi}^e)$$

Environmental
flux

Mass
flux



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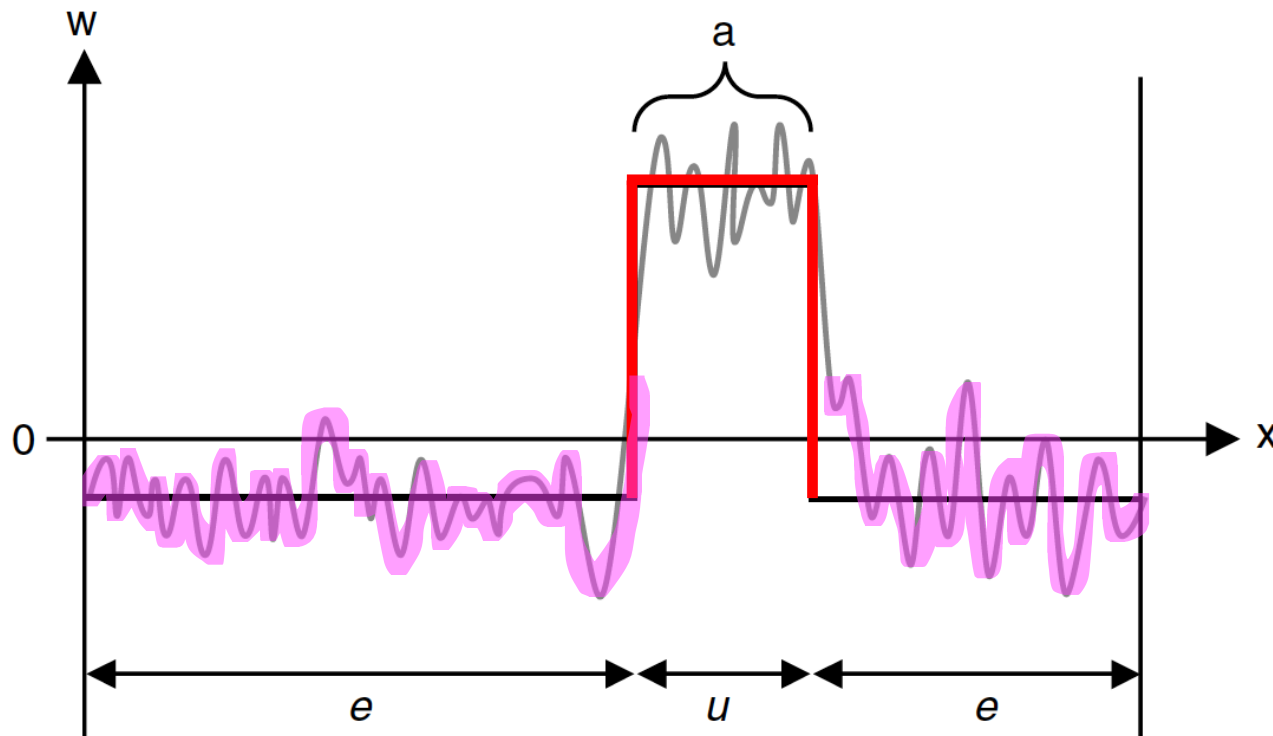
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Environmental
flux

Mass
flux



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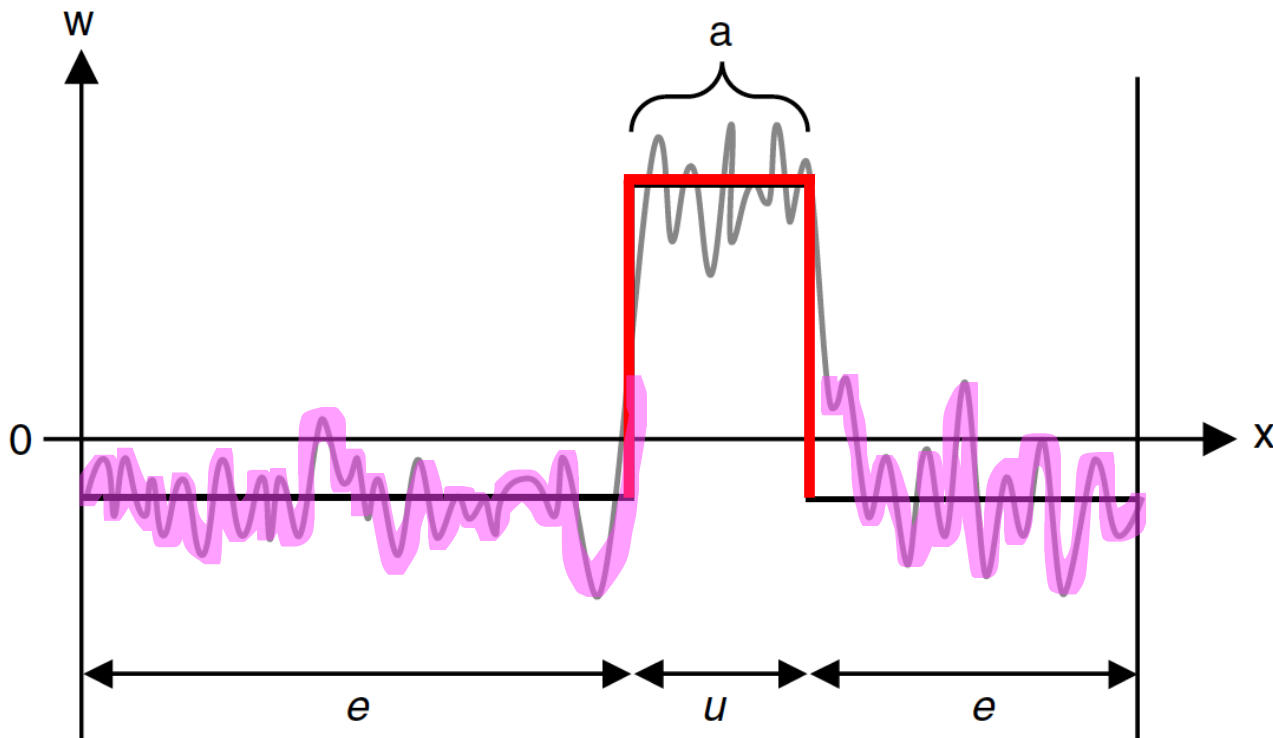
2. Environmental flux is given by K-diffusion:

$$(1 - a)\overline{\phi_e'w'} = -K_\phi \frac{\partial \phi}{\partial z}$$

'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

Total turbulent flux of ϕ :

$$\overline{\phi'w'} = \underbrace{-K_\phi \frac{\partial \phi}{\partial z}}_{\text{Environmental flux}} + \underbrace{a(\overline{w}^u - \overline{w})}_{\text{Mass flux}} (\overline{\phi}^u - \overline{\phi}^e)$$



Assumptions made:

1. Area of strongest updraft is small compared with the environment ($a \ll 1$).

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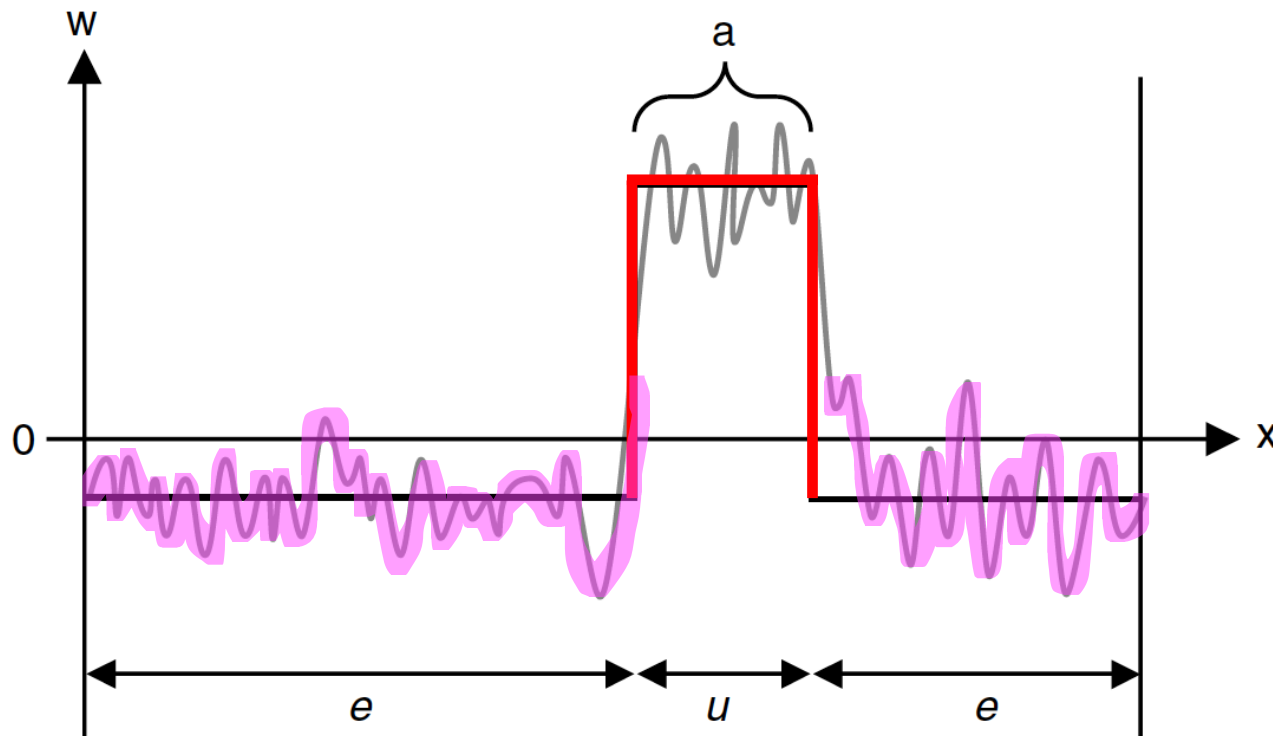
Total turbulent flux of ϕ :

$$\overline{\phi'w'} = -K_\phi \frac{\partial \phi}{\partial z} + M(\overline{\phi^u} - \overline{\phi^e})$$

Environmental
flux

Mass
flux

$$M = a(\overline{w^u} - \overline{w})$$



Assumptions made:

1. Area of strongest updraft is small compared with the environment ($a \ll 1$).

Subcore flux is neglected

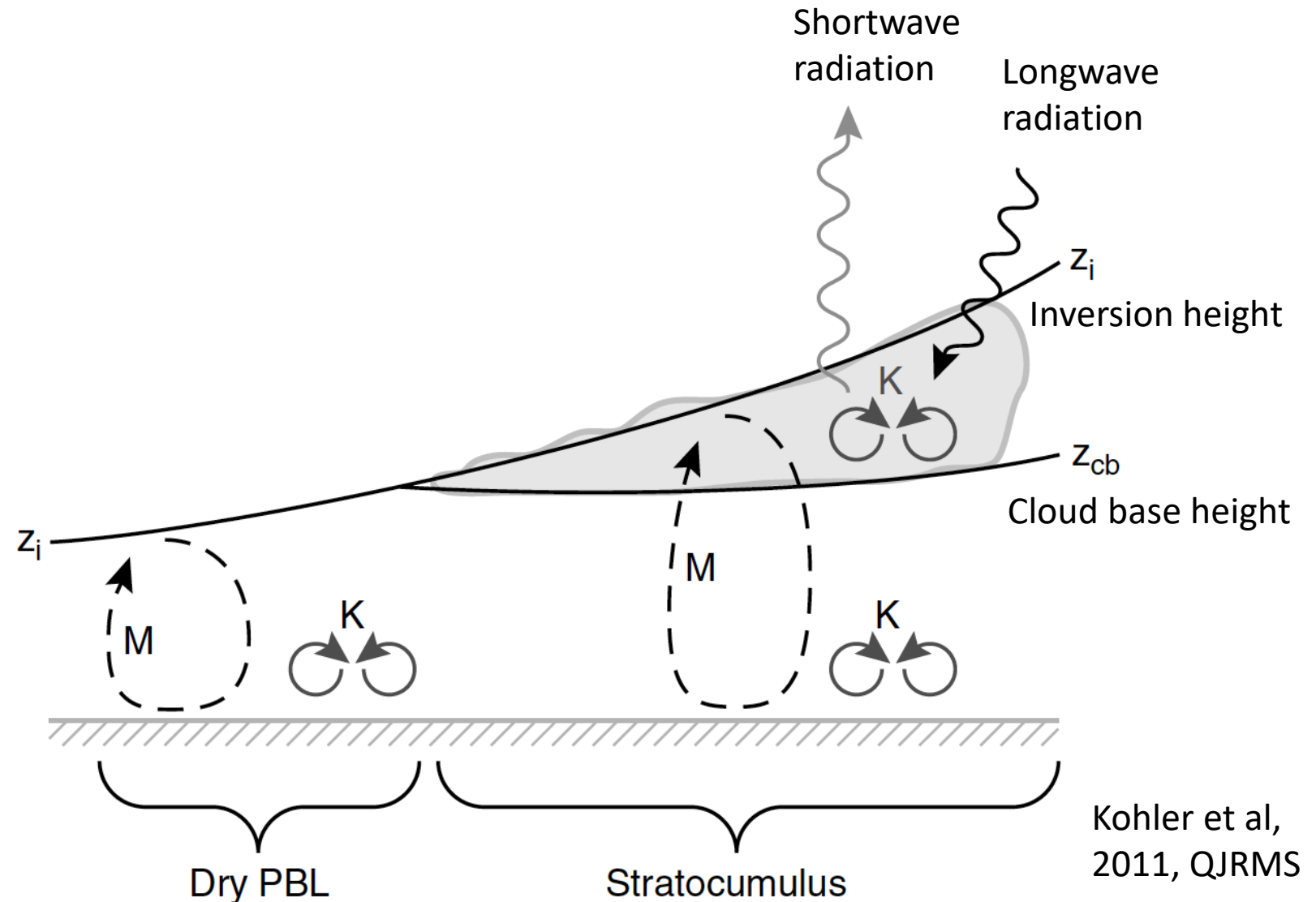
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'Non-Local' turbulence: eddy-diffusivity mass-flux (EDMF)

The surface mass flux (M) is initialised at the first model level

The mass flux profile then depends on the inversion height (z_i) or the cloud base height (z_{cb})

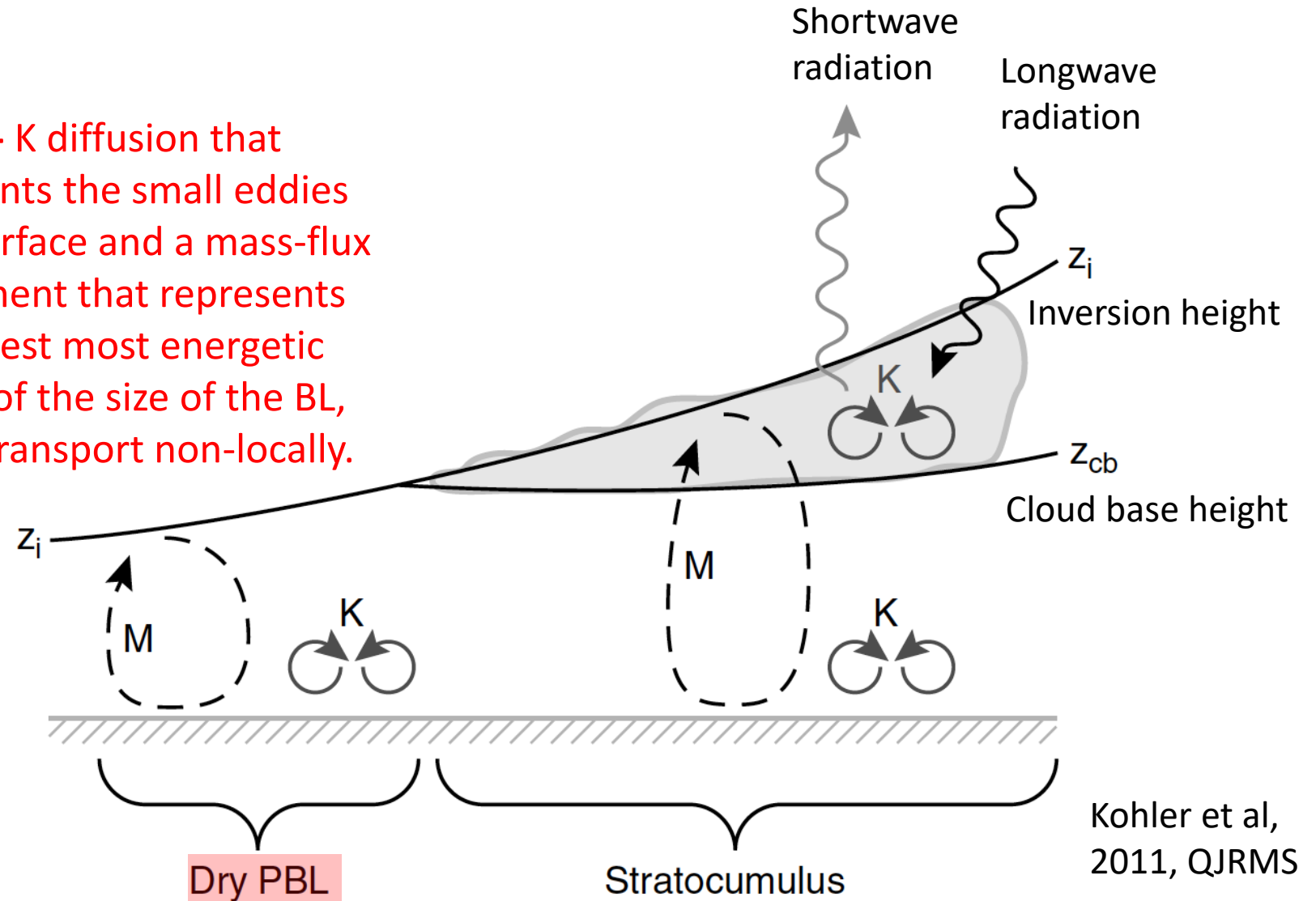


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Dry BL - K diffusion that represents the small eddies from surface and a mass-flux component that represents the largest most energetic eddies of the size of the BL, which transport non-locally.



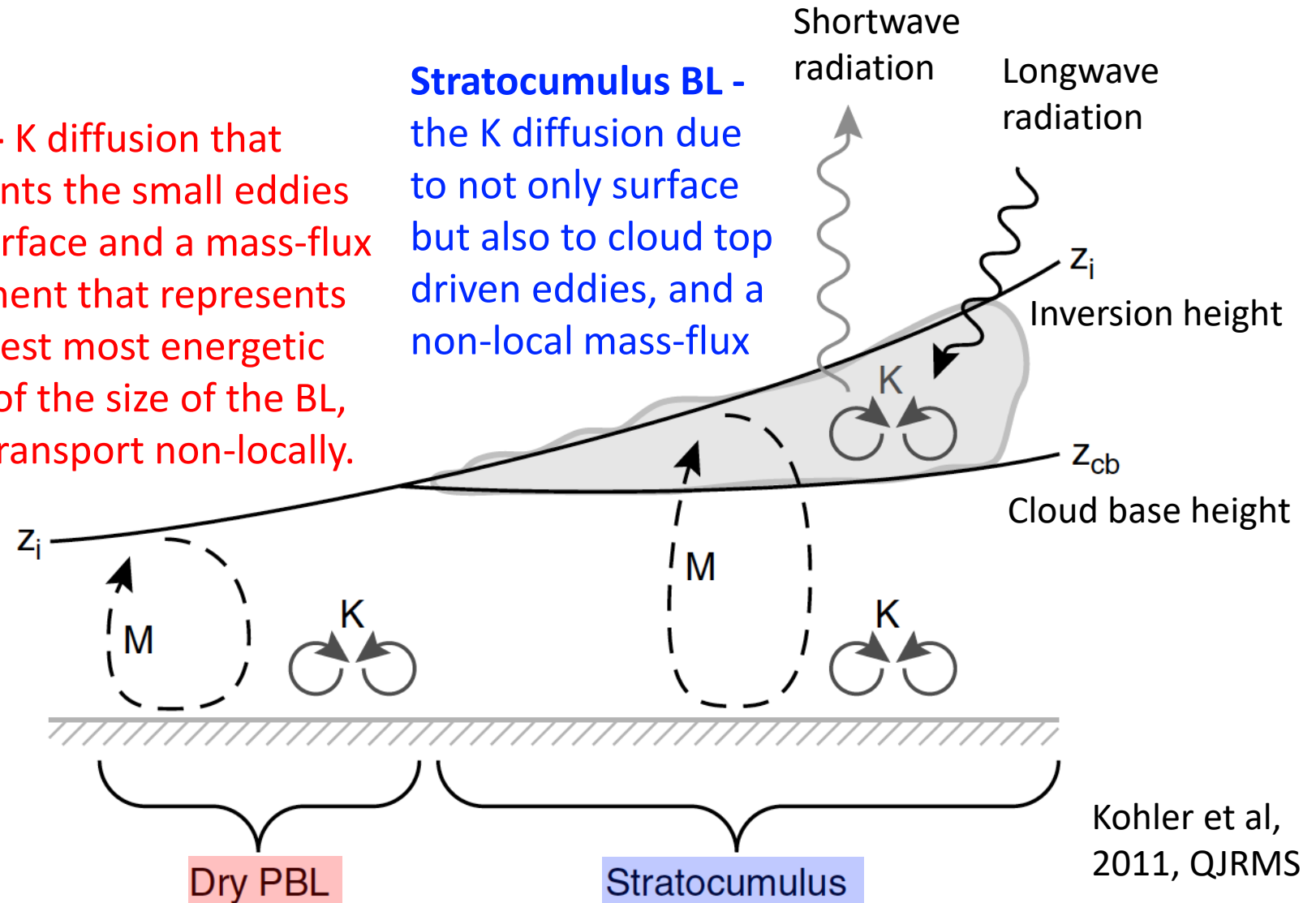
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Dry BL - K diffusion that represents the small eddies from surface and a mass-flux component that represents the largest most energetic eddies of the size of the BL, which transport non-locally.

Stratocumulus BL - the K diffusion due to not only surface but also to cloud top driven eddies, and a non-local mass-flux



Kohler et al, 2011, QJRMS

Summary of fundamental concepts

- **Local turbulence closure:**
 - Assumes local turbulent fluxes can be determined by a K-profile and the background gradients
 - Concept of an eddy lengthscale is used to determine the turbulent mixing
 - Lengthscale depends on height above the surface and the stability
- **MO surface layer similarity theory:**
 - Possible to relate the surface fluxes and near-surface gradients through universal functions
 - Functions depend on the Obukhov length (measure of surface stability)
- **Roughness length:**
 - Assumed to be a property of the surface roughness elements (e.g. vegetation / wave height)
- **Non-local turbulence (EDMF):**
 - Assumes that areas of strongest updrafts are small compared with environment
 - Allows convective mixing in well-mixed environments with small gradients