Discontinuous Higher Order Discretization Methods

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Numerical Methods for Numerical Weather Prediction ECMWF Training Course

November 2024

What are Higher Order Methods?

Definition

Higher order methods have truncation errors exceeding 2

• Fourth order finite-difference:

$$\frac{\partial u}{\partial x}\Big|_{x_i} = \frac{-u_{i+2} + 8u_{i+1} - 8u_{i-1} + u_{i-2}}{12\Delta x} + \frac{\Delta x^4}{30} \left. \frac{\partial^5 u}{\partial x^5} \right|_{x_i} + \dots$$

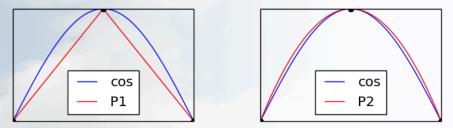
• The spectral method is of an "infinite order" $\partial^{p} u$ $||u - u_{\text{exact}}|| = O(N^{-p}), \quad N \to \infty, \quad \text{non-continuous in}$ дхр ⊖–1st order 3 2nd order 10^{-2} Exact 2nd O Central 4th O Central 10 4th O Pade 2 10 b 10-8 h, 10-1 10^{-1} 10^{-1} 10-3 10^{-1} 10^{-4} 10^{-2} 100 0 ó 2 h -- grid spacing hk

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Why Higher Order Methods?

Compare cos function, approximated by 3 points



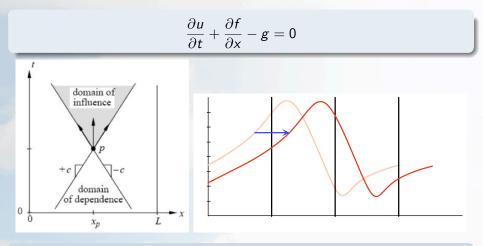
Can we not just add more points?

Higher-order methods when:

- High accuracy is required (increasingly so)
- Long time integration is required
- Memory becomes a bottleneck
- Scalability on parallel computers is important



Hyperbolic Conservation Laws



Conservation:

Flux going out of one cell = Flux entering the next

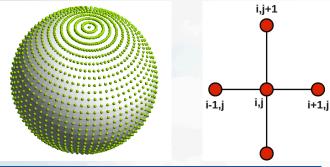


Higher-Order Finite Difference

Fourth order Finite difference:

$$\frac{\partial u_i}{\partial t} = -\left(\frac{-f_{i+2} + 8f_{i+1} - 8f_{i-1} + f_{i-2}}{12\Delta x}\right) + g_i$$

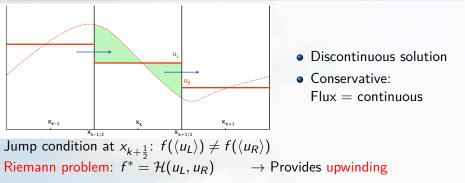
- Very fast, 5-point stencils
- Decoupling of domain in subdomains
- Structured grids
- Unnecessary small grid-spacing at higher latitudes



Finite Volume method

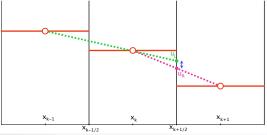
Integrated equation

$$\int \left(\frac{\partial u}{\partial t} + \frac{\partial f(u, x)}{\partial x} - g\right) dx = 0$$
$$\frac{\partial \langle u \rangle_k}{\partial t} + \frac{1}{\Delta x_k} \left[f^*\right]_{x_{k-\frac{1}{2}}}^{x_{k+\frac{1}{2}}} - \langle g \rangle = 0$$

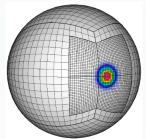




Second order Finite Volume Method



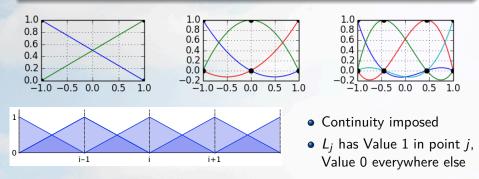
- Complex geometries on unstructured meshes
- Nested adaptive meshes
- Solution is defined in local manner
- Decoupling of domain in subdomains
- Natural upwinding couples cells
- Higher-order (>2) tedious and costly (extended stencils)
- Grid smoothness requirements



Finite Element Method – Continuous Galerkin

Equation is satisfied in global sense with solution defined nonlocally

$$\int \left(\frac{\partial u_h}{\partial t} + \frac{\partial f_h}{\partial x} - g\right) L_j(x) dx = 0, \qquad u_h(x) = \sum_k^N u_k L_k(x)$$





Global system of equations:

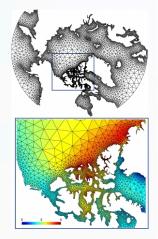
$$M \cdot rac{d\mathbf{u}_h}{dt} + S \cdot \mathbf{f}_h = M \cdot \mathbf{g}_h$$

Mass matrix M :

Stiffness matrix S :

$$M_{ij} = \int_{\Omega} L_i(x) L_j(x) dx$$
$$S_{ij} = \int_{\Omega} L_i(x) \frac{dL_j(x)}{dx} dx$$

- High-order accuracy with compact flexible elements
- Complex geometries on unstructured meshes
- Implicit in time (Linear System Solver)
- Not well suited for problems with direction
- Everything is coupled through Mass matrix





Discontinuous Higher-Order Methods

We want a method that combines

- the flexibility of high-order elements of FEM
- the locality and scalability of FVM

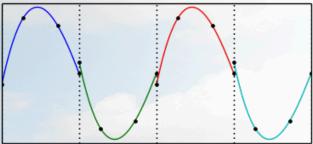
There exists a "family" of discontinuous higher-order methods with exactly these components

- Discontinuous Galerkin Method
- Spectral Volume Method
- Spectral Difference Method
- Flux Correction Method



Idea behind Discontinuous Higher-Order Methods

- Solution is described within one element as a high-order function (borrowed from Finite Element Method)
 - Polynomial of order P
 - Fourier series
 - Taylor series: $\langle u \rangle$, $\frac{\partial u}{\partial x}$, $\frac{\partial^2 u}{\partial x^2}$, ...
- Solution is defined locally on a per element basis
- Solution is not continuous across elements
- Flux is to be made continuous with Riemann solver (borrowed from Finite Volume Method)



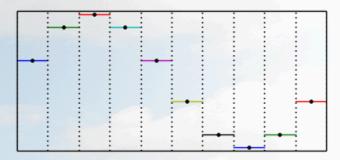
P3 basis functions



Observations

- Duplicated points at element interfaces (= more work)
- Solution does not look too nice as it is discontinuous
- Discontinuity does not affect high-order accuracy
- Discontinuity decouples elements (boundary conditions)
- Parallel efficiency outweighs more work

Interestingly: 1st order corresponds to Standard Finite Volume

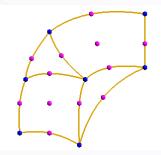


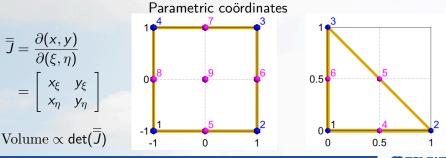
P0 basis functions



High-Order elements

- Extra points inside an element
- Effective increase in resolution
- Curved elements can align with coast lines
- Local mapping to standard element in parametric coördinates





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Lagrange polynomials

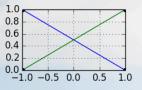
Interpolation

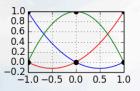
$$q(\xi) = \sum_{j=1}^{N} Q_j L_j(\xi)$$
 with $L_j(\xi) = \prod_{k \neq j}^{N} \frac{\xi - \xi_k}{\xi_j - \xi_k}$

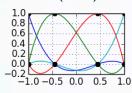
P1 (N=2)











Differentiation

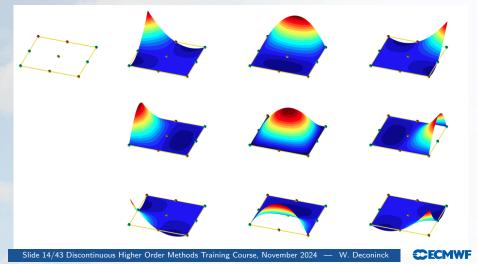
$$\frac{\partial q}{\partial \xi}(\xi) = \sum_{j=1}^{N} Q_j \ \frac{\partial L_j}{\partial \xi}(\xi) \qquad \text{with} \qquad \frac{\partial L_j}{\partial \xi}(\xi) = \sum_{\substack{i \neq j}}^{N} \frac{1}{\xi_j - \xi_i} \prod_{\substack{k \neq i \\ k \neq i}}^{N} \frac{\xi - \xi_k}{\xi_j - \xi_k}$$



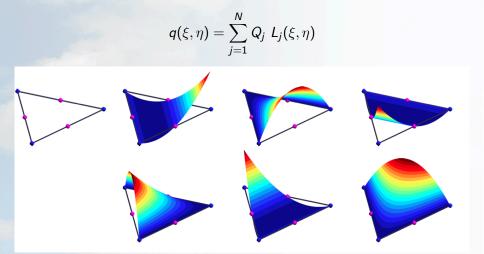
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Quadrilateral P2 (N=9)

$$q(\xi,\eta) = \sum_{j=1}^{N} Q_j L_j(\xi,\eta)$$



Triangle P2 (N=6)



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Element Integrals using quadrature

A quadrature rule approximates an integral using a weighted sum:

$$\int_{-1}^{+1} f(x) dx \approx \sum_{k=1}^{n} w_k^{\text{quad}} f(x_k^{\text{quad}})$$

x_k^{quad} are quadrature points
 w_k^{quad} are quadrature weights

One of the most widely used families of quadrature rules is Gauss-Legendre quadrature:

- Gauss-Legendre quadrature rule with *n* points and *n* weights can integrate a polynomial of degree 2n 1 exactly!
- x_k are distributed like the roots of the Legendre polynomial $P_n(x)$

•
$$w_k$$
 are then: $w_k = \frac{2}{(1-x_k^2)P'_n(x_k)^2}$

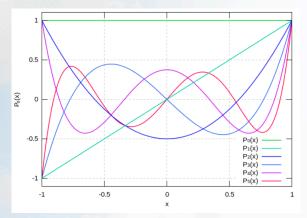


Legendre polynomials:

$$P_0(x) = 1, \qquad P_1(x) = x,$$

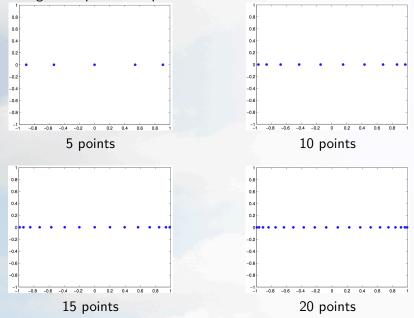
$$P_n(x) = \frac{2n-1}{n} P_{n-1}(x) x - \frac{n-1}{n} P_{n-2}(x)$$

$$P'_n(x) = \frac{n}{1-x^2} (P_{n-1}(x) - P_n(x) x)$$



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Gauss-Legendre quadrature points clustered towards ± 1 :



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The Gauss-Legendre quadrature points and weights have been extensively tabulated for $x \in [-1, 1]$

Number of points (n)	Quadrature points	Quadrature weights
1	0	2
2	$-1/\sqrt{3}, 1/\sqrt{3}$	1,1
3	$-\sqrt{3/5}, 0, \sqrt{3/5}$	5/9,8/9,5/9
:	:	:
	•	· ·

quadrature.py

: python-program provides points/weights with $x \in [-1, 1]$ for any n

Useful for exact integration of Lagrange
polynomials.
First interpolate to quadrature points!

n	2 <i>n</i> - 1
1	\leq P1
2	\leq P3
3	\leq P5



A Discontinuous Galerkin scheme

Deriving the DG formulation

$$\frac{\partial u}{\partial t} + \boldsymbol{\nabla} \cdot \boldsymbol{f} = 0$$

Integrate over entire domain Ω :

$$\int_{\Omega} \left(\frac{\partial u_h}{\partial t} + \boldsymbol{\nabla} \cdot \boldsymbol{f}_h \right) L_i(\boldsymbol{x}) d\boldsymbol{x} = 0$$

Rewrite as sum of element integration:

$$\sum_{e} \left(\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} + \int_{e} \nabla \cdot \mathbf{f}_{h} L_{i}(\mathbf{x}) d\mathbf{x} \right) = 0$$

Integrating by parts:

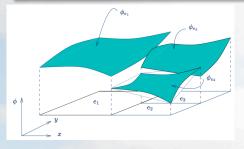
$$\sum_{e} \left(\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} + \oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*} \cdot \mathbf{n} d\mathbf{x} - \int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f} d\mathbf{x} \right) = 0$$



$$\sum_{e} \left(\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} + \oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*} \cdot \mathbf{n} d\mathbf{x} - \int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f} d\mathbf{x} \right) = 0$$

This can be satisfied for each element locally:

$$\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} + \oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*} \cdot \mathbf{n} d\mathbf{x} - \int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f} d\mathbf{x} = 0$$



Riemann problem:

 u_h is discontinuous at interfaces. We need conservation. Numerical flux function f^* must be unique and provides element coupling



Numerical Flux

Question: How should we choose f^* on the "faces" of an element?

Answer: Just like in FV, numerical flux on a face should depend on data in the two neighbouring elements.

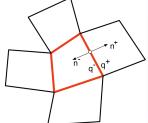
Let q^- (resp. q^+) denote the value of q on the interior (resp. exterior) face of an element

Let n^+ (resp. n^-) denote the outward normal vector on the face of the "local" (resp. "neighbour") element. Hence $n^- = -n^+$

Define "average" and "jump" operators:

$$\{\!\!\{q\}\!\!\} \equiv rac{q^- + q^+}{2}$$

 $[\![q]\!] \equiv \mathbf{n}^- q^- + \mathbf{n}^+ q^+ = \mathbf{n}^- (q^- - q^+)$





Numerical Flux

Roe scheme:

$$\mathbf{f}^* = \{\!\!\{\mathbf{f}\}\!\!\} + \frac{1}{2} |A| [\![u]\!] \quad \text{with} \quad A \equiv \frac{\partial \mathbf{f}}{\partial u}$$

Rusanov scheme:

$$f^* = \{\!\!\{f\}\!\!\} + \frac{1}{2}\lambda_{\max} [\![u]\!]$$
 with $\lambda_{\max} \equiv \max$ wave speed

Consider 1D linear advection: f = au, and a is advection speed

$$f^* = \frac{1}{2}(au^- + au^+) + \frac{|a|}{2}(u^- - u^+)$$
$$= u^-(\frac{a}{2} + \frac{|a|}{2}) + u^+(\frac{a}{2} - \frac{|a|}{2})$$
$$= \begin{cases} au^- & \text{if } a > 0\\ au^+ & \text{if } a < 0 \end{cases}$$



Numerical Flux Properties

- Stability: upwind according to flow direction
- Conservative: **f**^{*} is same computed when computed from the perspective of the neighbour element
- Consistent: $f^* \to f$ when $\llbracket u \rrbracket \to 0$
- Rusanov scheme is much more dissipative than Roe scheme

Finite Volume

The jump $\llbracket u \rrbracket$ is usually large, and Roe scheme is preferred.

Discontinuous Higher-Order methods

The jump $[\![u]\!]$ can be very small, making the cheaper Rusanov scheme an attractive choice.



Back to the DG scheme

$$\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} + \oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*} \cdot \mathbf{n} d\mathbf{x} - \int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f} d\mathbf{x} = 0$$

Consider the special P0 case where $L_i(\mathbf{x}) = 1$, and thus $\nabla L_i(\mathbf{x}) = 0$:

$$\int_{e} \frac{\partial u_{h}}{\partial t} d\mathbf{x} + \oint_{\partial e} \mathbf{f}^{*} \cdot \mathbf{n} d\mathbf{x} = 0$$

This is the definition of the Finite Volume scheme!

Although we started from the variational formulation like the Finite Element Method, the Discontinuous Galerkin Method can be reinterpreted as an extention of the Finite Volume Method



Implementing a DG scheme

$$\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} = \int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f}(\mathbf{x}) d\mathbf{x} - \oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*}(\mathbf{x}) \cdot \mathbf{n} d\mathbf{x}$$
$$u_{h}(\mathbf{x}, t) = \sum_{j=1}^{N} u_{j}(t) L_{j}(\mathbf{x})$$
$$\sum_{j=1}^{N} \underbrace{\int_{e} L_{i}(\mathbf{x}) L_{j}(\mathbf{x}) d\mathbf{x}}_{M_{ij}} \frac{\partial u_{j}}{\partial t} = \underbrace{\int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f}(\mathbf{x}) d\mathbf{x}}_{RHS_{i}^{l}} - \underbrace{\oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*}(\mathbf{x}) \cdot \mathbf{n} d\mathbf{x}}_{RHS_{i}^{l}}$$
$$\mathsf{M}_{e} \frac{\partial \mathsf{U}_{e}}{\partial t} = \mathsf{RHS}_{e}^{l} - \mathsf{RHS}_{e}^{l}$$

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$$\mathsf{M}_{e}\frac{\partial \mathsf{U}_{e}}{\partial t} = \mathsf{RHS}'_{e} - \mathsf{RHS}''_{e}$$

Mass matrix

$$M_{ij}^e = \int_e L_i(\mathbf{x}) L_j(\mathbf{x}) d\mathbf{x}$$

Computation in practice

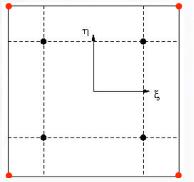
Transform to parametric coördinates

$$M_{ij}^{e} = \int_{e} L_{i}(\xi) L_{j}(\xi) \left| \frac{dx}{d\xi} \right| d\xi$$

Gaussian Quadrature

$$M^e_{ij} = \sum_q^{N_q} w_q \ L_i(\xi_q) \ L_j(\xi_q) \ |J_q|$$





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First RHS term

$$\operatorname{RHS}_{i}^{I} = \int_{e} \boldsymbol{\nabla} L_{i}(\boldsymbol{x}) \cdot \boldsymbol{f}(\boldsymbol{x}) \, d\boldsymbol{x}$$

Computation in practice

Transform to parametric coördinates

$$\operatorname{RHS}_{i}^{\prime} = \int_{e} \nabla L_{i}(\xi) \overline{\overline{J}}^{-1} \cdot f(\xi) |J| d\xi$$

Gaussian Quadrature

$$\operatorname{RHS}_{i}^{I} = \sum_{q}^{N_{q}} w_{q} \, \boldsymbol{\nabla} L_{i}(\boldsymbol{\xi}_{q}) \, |J_{q}| \, \overline{\overline{J}}_{q}^{-1} \cdot \boldsymbol{f}(\boldsymbol{\xi}_{q})$$

Approximation of order of scheme: $f(\xi) \approx \sum_{j=1}^{N} L_j(\xi) f(u_j)$

$$\operatorname{RHS}_{i}^{\prime} \approx \sum_{j=1}^{N} \underbrace{\sum_{q}^{N_{q}} w_{q} L_{i}(\xi_{q}) \nabla L_{i}(\xi_{q}) |J_{q}| \overline{\overline{J}}_{q}^{-1}}_{q} \cdot \boldsymbol{f}_{j}$$

 S_{ij} RHS^{*I*}_{*e*} \approx S_{*e*} F_{*e*}

Stiffness or Advection matrix

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 $\mathsf{M}_{e}\frac{\partial \mathsf{U}_{e}}{\partial t} = \mathsf{RHS}_{e}^{\prime} - \mathsf{RHS}_{e}^{\prime\prime}$

Second RHS term

$$\operatorname{RHS}_{i}^{\prime\prime} = \oint_{\partial e} L_{i}(\boldsymbol{x}) \boldsymbol{f}^{*}(\boldsymbol{x}) \cdot \boldsymbol{n} \, d\boldsymbol{x}$$

Computation in practice

Transform to parametric coördinates

$$\operatorname{RHS}_{i}^{II} = \sum_{f=1}^{N_{f}} \int_{\partial e_{f}} L_{i}(\boldsymbol{\xi}) \boldsymbol{f}^{*}(\boldsymbol{\xi}) \cdot \boldsymbol{n} |J_{f}| d\boldsymbol{\xi}$$

Example in 1D

$$\operatorname{RHS}_{i}^{\prime\prime} = L_{i}(\xi_{L}) \boldsymbol{f}^{*}(\xi_{L}) \cdot (-1) + L_{i}(\xi_{R}) \boldsymbol{f}^{*}(\xi_{R}) \cdot (+1)$$
$$\operatorname{RHS}_{i}^{\prime\prime} = [L_{i}(\xi_{L}) \quad L_{i}(\xi_{R})] \cdot \begin{bmatrix} -\boldsymbol{f}^{*}(\xi_{L}) \\ +\boldsymbol{f}^{*}(\xi_{R}) \end{bmatrix}$$

$$\mathbf{RHS}_{e}^{\prime\prime} = \mathbf{H}_{e} \ \mathbf{Fn}_{e}^{*}$$

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 $\mathsf{M}_{e}\frac{\partial \mathsf{U}_{e}}{\partial t} = \mathsf{RHS}_{e}^{I} - \mathsf{RHS}_{e}^{II}$

Collecting the pieces

$$\mathsf{M}_{e}\frac{\partial \mathsf{U}_{e}}{\partial t} = \mathsf{RHS}_{e}^{\prime} - \mathsf{RHS}_{e}^{\prime\prime}$$

$$\int_{e} \frac{\partial u_{h}}{\partial t} L_{i}(\mathbf{x}) d\mathbf{x} = \int_{e} \nabla L_{i}(\mathbf{x}) \cdot \mathbf{f}(\mathbf{x}) d\mathbf{x} - \oint_{\partial e} L_{i}(\mathbf{x}) \mathbf{f}^{*}(\mathbf{x}) \cdot \mathbf{n} d\mathbf{x}$$

Implemented as matrix products

$$\mathbf{M}_{e} \frac{\partial \mathbf{U}_{e}}{\partial t} = \mathbf{S}_{e} \ \mathbf{F}_{e} - \mathbf{H}_{e} \ \mathbf{Fn}_{e}^{*}$$
$$\frac{\partial \mathbf{U}_{e}}{\partial t} = \mathbf{M}_{e}^{-1} \ \mathbf{S}_{e} \ \mathbf{F}_{e} - \mathbf{M}_{e}^{-1} \ \mathbf{H}_{e} \ \mathbf{Fn}_{e}^{*}$$
$$\frac{\partial \mathbf{U}_{e}}{\partial t} = \mathbf{Ds}_{e} \ \mathbf{F}_{e} - \mathbf{Dh}_{e} \ \mathbf{Fn}_{e}^{*}$$

 $\mathbf{U}_{e} = [u_{1}, u_{2}, u_{3}, \dots, u_{N}] \qquad \mathbf{F}_{e} = [f(u_{1}), f(u_{2}), f(u_{3}), \dots, f(u_{N})]$



Demonstration 1D DGM

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Spectral Difference Method

Why this name?

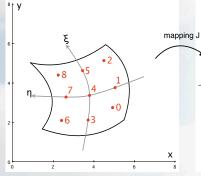
- Spectral: Higher-Order solution can be described as a Fourier Series
- Difference: Equations are solved in differential form, like Finite Difference

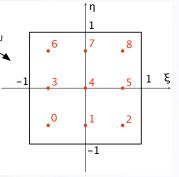
Some properties

- \bullet Differential form of equations \rightarrow no quadrature necessary
- Unstructured grids / Complex geometries
- Compact stencil
- Shape functions provide higher order
- Upwinding between cells through Riemann solver
- Very intuitive approach



Spectral Difference method

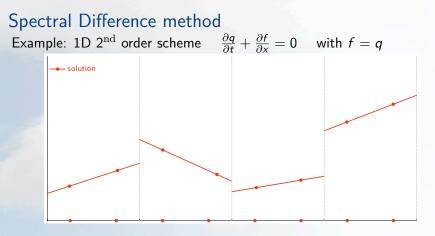




$$\begin{aligned} \frac{\partial q}{\partial t} + \nabla \cdot \mathbf{f} &= 0 & \frac{\partial \widetilde{q}}{\partial t} + \widetilde{\nabla} \cdot \widetilde{\mathbf{f}} &= 0 \\ \text{with mapping } \overline{\overline{J}} &= \partial \overline{x} / \partial \overline{\xi} \\ \widetilde{q} &= |J| \ q & \widetilde{\mathbf{f}} &= \begin{bmatrix} \widetilde{f}_{\xi} \\ \widetilde{f}_{\eta} \end{bmatrix} = |J| \ \overline{\overline{J}}^{-1} \ \mathbf{f} \end{aligned}$$

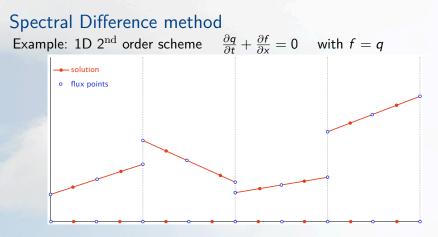
 \tilde{f}_{c}





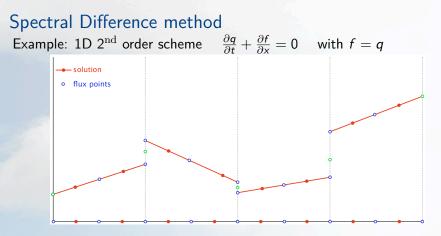
- Solution $q(\xi)$ is discontinuous and linear
- Goal is to get $\frac{\partial}{\partial \xi}$ to 2^{nd} order accuracy





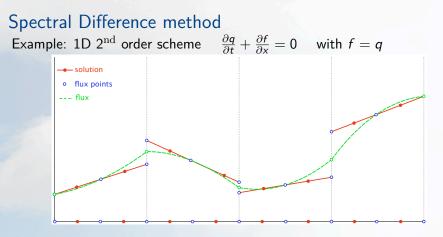
- Extrapolate solution $q(\xi)$ to "flux points"
- Compute flux
- Compute Riemann flux for conservation and upwinding between cells





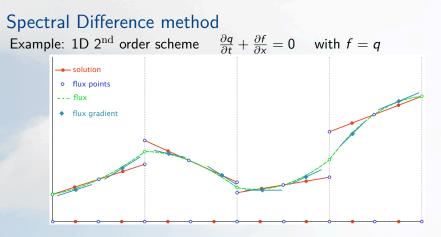
- Extrapolate solution $q(\xi)$ to "flux points"
- Compute flux
- Compute Riemann flux for conservation and upwinding between cells





- Flux is now a parabolic function
- Compute gradient of parabolic function in "solution points"





- Flux is now a parabolic function
- Compute gradient of parabolic function in "solution points"



Stability of the Spectral Difference Method

Question:

- Where should we put the solution points?
- Where should we put the flux points?

Answer:

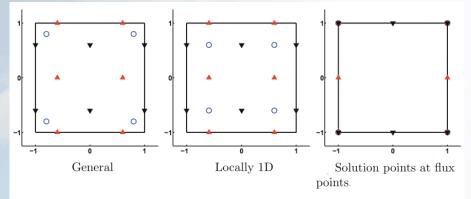
- Free to choose location of solution points
- Flux points however not:
 - Points on interface for element coupling
 - Stability analysis required (not covered)
 - One more point than solution points (in 1D)

Flux point location

Roots of Legendre polynomial plus [$\xi = -1, \ \xi = +1$]

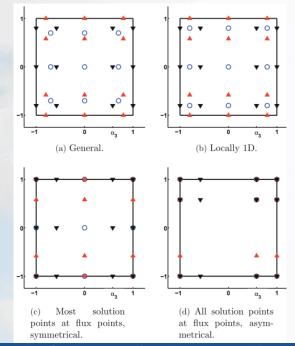


Solution / Flux Point distributions for SD



Second-order quadrilateral SD cells. Solution points (\bigcirc) and ξ_1 - (\triangledown) and ξ_2 -flux points (\blacktriangle).





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CECMWF

Implementing a SD method

 Interpolate solution to all flux points (could be optimized depending on solution point distribution)

$$q_f = \sum_{j=1}^N q_j \ L_j^{
m sol}(\boldsymbol{\xi}_f) \qquad o \ Q_{
m flxpts}^e = {\sf I}_f Q^e$$

Ocompute numerical flux in interface flux points

$$\tilde{\mathbf{F}}_{\text{interface}}^{e} = |J| \overline{\overline{J}}^{-1} \mathbf{f}^{*}$$

Ocompute fluxes in internal flux points

$$ilde{\mathsf{F}}^{e}_{ ext{internal}} = |J| \; \overline{\overline{J}}^{-1} \; {m{f}}(Q^{e}_{ ext{flxpts}})$$

Ompute flux divergence

$$\frac{\partial \tilde{\mathbf{f}}}{\partial \xi} = \sum_{j=1}^{N_f} \tilde{\mathbf{f}}_j \ \frac{\partial L_j^{\text{fix}}(\boldsymbol{\xi}_f)}{\partial \xi} \qquad \rightarrow \tilde{\boldsymbol{\nabla}} \cdot \tilde{\mathbf{F}}^e = \tilde{\mathbf{D}} \ \tilde{\mathbf{F}}^e$$

Opdate solution:

$$\frac{\partial Q^e}{\partial t} = \frac{1}{|J|} \tilde{\mathbf{D}} \; \tilde{\mathbf{F}}^e$$



Demonstration 1D SDM

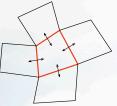
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Parallel efficiency

Discontinuous Higher-Order methods offer huge potential

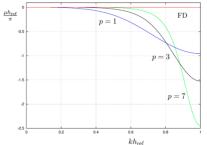
- Matrix multiplications for near peak FLOP-rates
 I have shown you can write the entire method in matrix-vector notation
- Avoiding global communication Every element acts as a standalone domain with boundary conditions

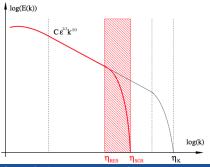


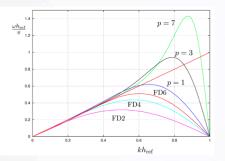
- Mapping of problem to nested hierarchical computer architectures
 - MPI distributed memory
 - OpenMP shared memory
 - Accelerators (e.g. GPU) matrix multiplications



Spectral properties







Properties depend on choices for numerical flux, shape functions

Numerical damping of high wave numbers could make the method suitable for Implicit LES!



Concluding

- Introduction to Higher-Order accuracy on unstructured meshes
- Implementations for hyperbolic conservation laws
- There is lots more to consider (diffusion terms, monotonicity, time stepping, curved elements)
- Parallel efficiency as main driving force
- Implicit LES properties are to be examined



References

- Hesthaven, J.S., Warburton, T.: Nodal Discontinuous Galerkin Methods — Algorithms, Analysis, and Applications
- Liu, Y., Vinokur, M., & Wang, Z. (2006). Spectral difference method for unstructured grids I: Basic formulation. Journal of Computational Physics.
- Dhatt, G., Touzot, G.: The Finite Element Method Displayed

